

## 9-3 Inductance

**Reading Assignment:** *pp. 290-286*

\* A transformer is an example of **mutual inductance**, where a time-varying current in **one** circuit (i.e., the primary) induces an emf voltage in **another** circuit (i.e., the secondary).

\* We likewise can have **self inductance**, where a time-varying current in a circuit induces an emf voltage within that **same** circuit!

In fact, we can create circuit structures where this induced emf will be **very large**—we call these circuit elements **inductors**!

**Q:** *So how do we **make** an inductor?*

**A:** Typically, an inductor is a **solenoid**!

**HO: Inductance**

**Example: The Inductance of a Solenoid**

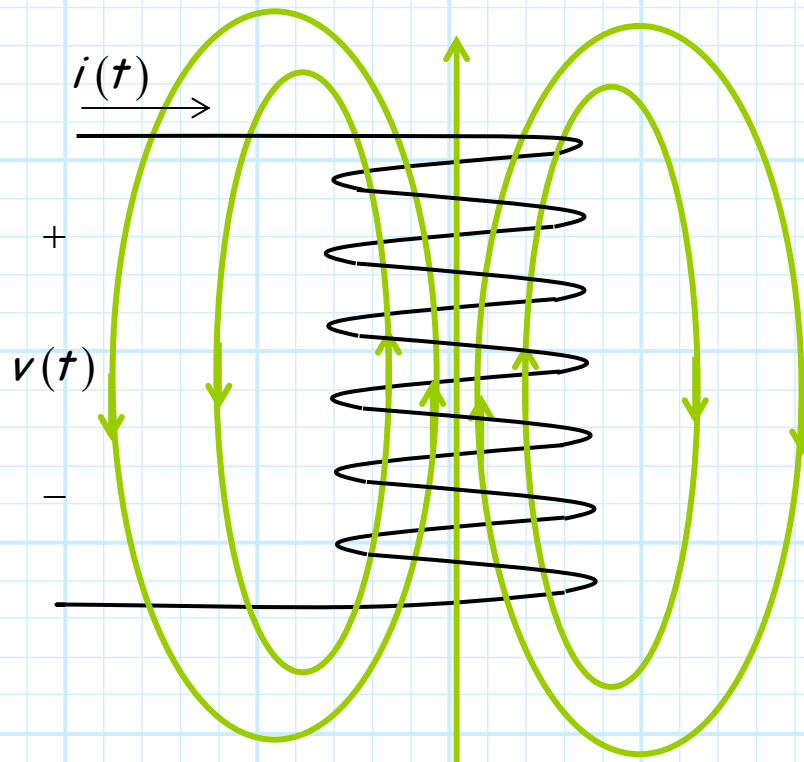
## Example: The Inductance of a Coaxial Transmission Line

Just like a capacitor, an inductor can **store energy!**

### HO: Energy and Magnetic Fields

# Inductance

Consider a **solenoid** with  $N$  turns:



The current  $i(t)$  in flowing in the wire will produce a time-varying magnetic flux density within the solenoid. This time-varying magnetic flux density will **induce a voltage**  $v(t)$  across the solenoid.

This voltage can be determined using **Faraday's Law**:

$$-\oint_{\mathcal{C}_1} \mathbf{E}(\vec{r}) \cdot d\vec{\ell} = \frac{\partial}{\partial t} \iint_{\mathcal{S}_1} \mathbf{B}(\vec{r}) \cdot d\vec{s}$$

Just like we determined for the **ideal transformer**, we find that:

$$-\oint_{C_1} \mathbf{E}(\vec{r}) \cdot d\vec{\ell} = v(t)$$

and that:

$$\begin{aligned} \frac{\partial}{\partial t} \iint_{S_1} \mathbf{B}(\vec{r}) \cdot d\vec{s} &= \frac{\partial}{\partial t} N \iint_{S_0} \mathbf{B}(\vec{r}) \cdot d\vec{s} \\ &= N \frac{\partial \Phi(t)}{\partial t} \end{aligned}$$

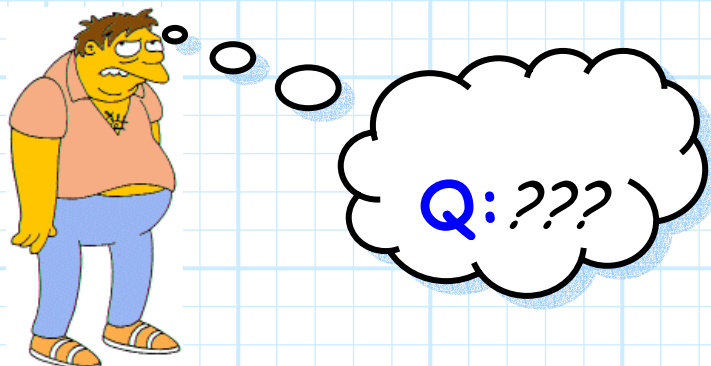
where  $S_0$  is the surface area of **one** loop.

Therefore, just as we determined for a transformer, Faraday's Law says that:

$$v(t) = N \frac{\partial \Phi(t)}{\partial t}$$

Now, let's **define** the product  $N \Phi(t)$  as:

$$N \Phi(t) \doteq \Lambda(t) = \text{flux linkages} \quad [\text{Webers}]$$



**A:** A magnetic flux of  $\Phi(t)$  Webers passes through **each and every** one of the  $N$  loops of the solenoid. We say therefore that each loop surrounds, or "**links**"  $\Phi(t)$  Webers of flux. If there are  $N$  loops, then the solenoid links a **total** of  $N \Phi(t)$  Webers of flux. We call therefore  $N \Phi(t)$  the total **flux linkages** surrounded by the solenoid.

Thus we can state our induced solenoid voltage as the time derivative of the flux linked by the solenoid:

$$v(t) = \frac{\partial \Lambda(t)}{\partial t}$$

Now, recall that current  $i(t)$  produced the magnetic flux density and thus the magnetic flux. As a result, we find that the current  $i(t)$  is **directly proportional** to the total flux linkages of the solenoid:

$$i(t) \propto \Lambda(t)$$

Lets define the **proportionality constant** as  $L$ , so that we can say:

$$\Lambda(t) = L i(t)$$

Since  $i(t)$  has units of amps and  $\Lambda(t)$  the units of Webers, the constant  $L$  must have units of **Webers/Amp**.

Taking the **time derivative** we thus find:

$$\frac{\partial \Lambda(t)}{\partial t} = L \frac{\partial i(t)}{\partial t}$$

Note we can now write the **induced voltage** as:

$$v(t) = L \frac{\partial i(t)}{\partial t}$$

**Q:** Look familiar?

**A:** *Of course, L is inductance!*

Inductance is therefore defined as the **ratio** of current  $i$  to the total flux linkages it creates!

$$L \doteq \frac{\Lambda}{i} = \text{inductance} \left[ \frac{\text{Webers}}{\text{Amp}} \right]$$

Inductance is obviously dependent on the **structure** of the device (e.g., number of loops, diameter, length).

By the way, we have another name for Webers/Amp—**Henries!**

$$\text{Henries} \doteq \frac{\text{Webers}}{\text{Ampere}}$$

# Example: The Inductance of a Solenoid

Many **inductors** used in electronic circuits are simply **solenoids**. Let's determine the **inductance** of this structure!

First, we recall that inductance is the **ratio** of the **current** and the **flux linkages** that the current produces:

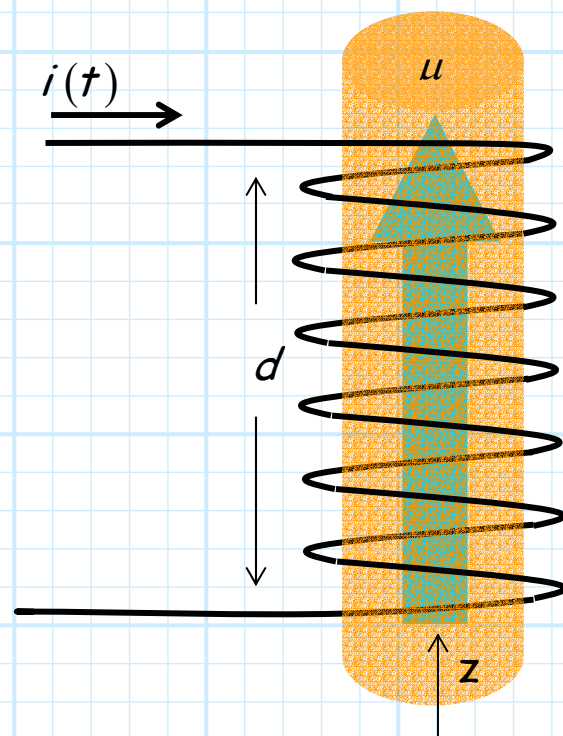
$$L \doteq \frac{\Lambda}{i} = \text{inductance} \left[ \frac{\text{Webers}}{\text{Amp}} \right]$$

The question then is, what is flux linkages  $\Lambda$  for a **solenoid**?

Recall that the magnetic flux density in the **interior** of a solenoid is:

$$\mathbf{B}(\vec{r}) \approx \frac{\mu N i}{d} \hat{a}_z$$

where  $N$  is the number of loops and  $d$  is the length of the solenoid.



The total **magnetic flux** flowing through the solenoid is therefore found by integrating across the **cross-section** of the solenoid:

$$\begin{aligned}\Phi &= \iint_S \mathbf{B}(\vec{r}) \cdot \overline{d\mathbf{s}} \\ &= \frac{\mu N i}{d} S\end{aligned}$$

where  $S$  is the cross-sectional area of the solenoid (e.g.,  $S = \pi a^2$  if solenoid is circular with radius  $a$ ).

Recall the total **flux linkage** is just the **product** of the **magnetic flux** and the **number of loops**:

$$\begin{aligned}\Lambda &= N\Phi \\ &= \frac{\mu N^2 S}{d} i\end{aligned}$$

Thus, we now find that the **inductance of a solenoid** is:

$$L = \frac{\Lambda}{i} = \frac{\mu N^2 S}{d}$$



Note if we wish to **increase** the inductance of this solenoid, we can either:

- 1) **Increase** the permeability  $\mu$  of the core material.
- 2) **Increase** the number of turns  $N$ .
- 3) **Increase** the cross-sectional area  $S$
- 4) **Decrease** the length  $d$  (while keeping  $N$  constant).

Note all of the derivations in this handout are derived from the solution to an **infinite** solenoid. As a result, they are **approximations**, but are typically accurate ones **provided** that:

$$d \gg \sqrt{S}$$

In other words, provided that the inductor **length** is significantly **greater** than its **radius**.

# The Inductance of a Coaxial Transmission Line

Recall that we earlier determined the **capacitance** (per unit length) of a **coaxial transmission line** to be:

$$\frac{C}{\ell} = \frac{2\pi\epsilon}{\ln[b/a]} \quad \left[ \frac{\text{farads}}{\text{meter}} \right]$$

We can likewise determine its **inductance** per unit length.

**Q:** *Yikes! How do we accomplish this? There are no loops in a coaxial line!*

**A:** True. We instead begin by determining the **energy stored** (per unit length) of a coax line.

Recall that the magnetic flux density **between** the inner and outer conductors of a coaxial line is:

$$\mathbf{B}(\vec{r}) = \frac{\mu I}{2\pi\rho} \hat{a}_\phi \quad (a < \rho < b)$$

Therefore the **magnetic field** within the line is:

$$\mathbf{H}(\vec{r}) = \frac{I}{2\pi\rho} \hat{a}_\phi \quad (a < \rho < b)$$

The **energy stored** in a length  $\ell$  of the coax line is therefore:

$$\begin{aligned} W_m &= \frac{1}{2} \iiint \mathbf{B} \cdot \mathbf{H} \, dv \\ &= \frac{\mu I^2}{8\pi^2} \int_0^\ell \int_a^b \int_0^{2\pi} \frac{1}{\rho^2} \hat{\mathbf{a}}_\phi \cdot \hat{\mathbf{a}}_\phi \, \rho \, d\rho \, d\phi \, dz \\ &= \frac{\mu I^2 \ell}{4\pi} \ln \left[ \frac{b}{a} \right] \end{aligned}$$

**Q:** *So what? We want to find the **inductance** of the line, not the energy stored in it!*

**A:** True. But recall inductance is **related** to stored energy as:

$$W_m = \frac{1}{2} LI^2$$

Or in other words:

$$L = \frac{2W_m}{I^2}$$

Using this expression, we find:

$$\begin{aligned} L &= \frac{2}{I^2} \left( \frac{\mu I^2 \ell}{4\pi} \ln \left[ \frac{b}{a} \right] \right) \\ &= \frac{\mu}{2\pi} \ln \left[ \frac{b}{a} \right] \ell \end{aligned}$$

Or, in other words, the **inductance per unit length** of a coax transmission line is:

$$\frac{L}{\ell} = \frac{\mu}{2\pi} \ln \left[ \frac{b}{a} \right] \quad \left[ \frac{\text{Henries}}{\text{m}} \right]$$

Note here that we did **not** consider the magnetic fields **within the conductors**. For most engineering applications (i.e., **time-varying**), we will find that the contribution of these fields are small and thus can be **neglected**.

# Energy and Magnetic Fields

Recall that the **energy stored** in an **electrostatic** system is:

$$W_e = \frac{1}{2} \iiint_V \rho_v(\vec{r}) V(\vec{r}) dv$$

or equivalently:

$$W_e = \frac{1}{2} \iiint_V \mathbf{D}(\vec{r}) \cdot \mathbf{E}(\vec{r}) dv$$

This led to the expression relating energy and **capacitance**:

$$W_e = \frac{1}{2} CV^2$$

We can similarly ask the question, how much **energy** is stored in a **magnetostatic** system?

Precisely the amount of **work** required to establish the **current density**  $\mathbf{J}(\vec{r})$ !

We find that the expressions for this work/energy are **analogous** to that of electrostatics. For example, we find that:

$$W_m = \frac{1}{2} \iiint_V \mathbf{J}(\bar{r}) \cdot \mathbf{A}(\bar{r}) dv$$

Therefore, we **again** find that energy stored is equal to the integration of the "product" of the **sources** (e.g.,  $\rho_v$  or  $\mathbf{J}$ ) and the **potential** function (e.g.,  $V$  or  $\mathbf{A}$ ).

Likewise, this energy can be expressed in terms of the two magnetic **fields**:

$$W_m = \frac{1}{2} \iiint_V \mathbf{B}(\bar{r}) \cdot \mathbf{H}(\bar{r}) dv$$

Therefore, we again find that energy stored is equal to the integration of the dot product of the **flux density** (e.g.,  $\mathbf{D}$  or  $\mathbf{B}$ ) and the other **field** (e.g.,  $\mathbf{E}$  or  $\mathbf{H}$ ).

We likewise find that this energy can be directly expressed for the energy stored by an **inductor**:

$$W_m = \frac{1}{2} LI^2$$

Look familiar ?