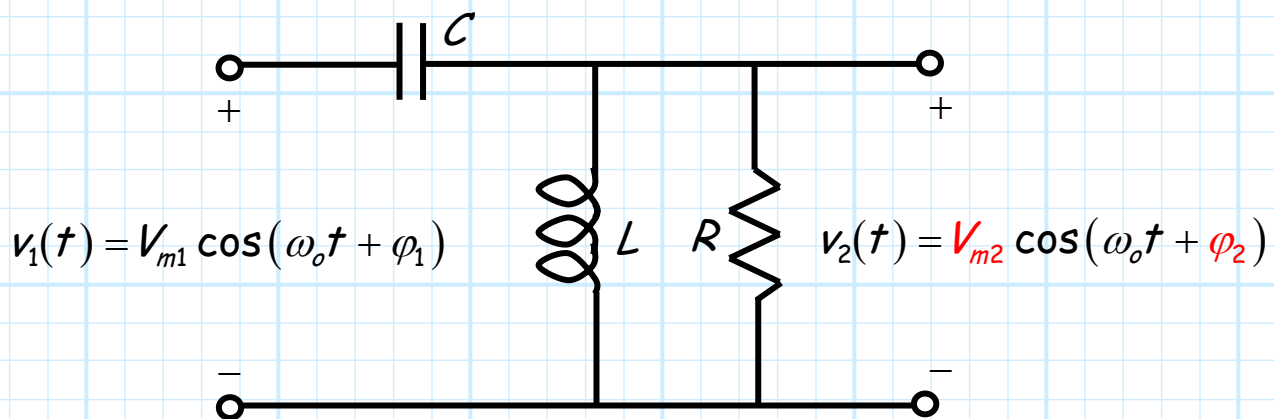


# A Complex Representation of Sinusoidal Functions

**Q:** So, you say (for example) if a linear two-port circuit is driven by a sinusoidal source with arbitrary frequency  $\omega_o$ , then the output will be identically sinusoidal, only with a different magnitude and relative phase.



How do we determine the unknown magnitude  $V_{m2}$  and phase  $\phi_2$  of this output?

**A:** Say the input and output are related by the impulse response  $g(t)$ :

$$v_2(t) = \mathcal{L}[v_1(t)] = \int_{-\infty}^t g(t-t') v_1(t') dt'$$

We now know that if the input were instead:

$$v_1(t) = e^{j\omega_o t}$$

then:

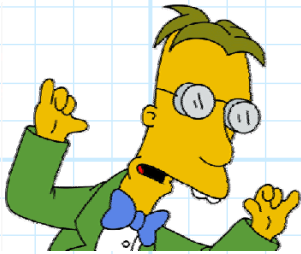
$$v_2(t) = \mathcal{L} \left[ e^{j\omega_0 t} \right] = G(\omega_0) e^{j\omega_0 t}$$

where:

$$G(\omega_0) \doteq \int_0^{\infty} g(t) e^{-j\omega_0 t} dt$$

Thus, we simply multiply the input  $v_1(t) = e^{j\omega_0 t}$  by the **complex** eigen value  $G(\omega_0)$  to determine the **complex** output  $v_2(t)$ :

$$v_2(t) = G(\omega_0) e^{j\omega_0 t}$$



**Q:** *You professors drive me crazy with all this math involving **complex** (i.e., real and imaginary) voltage functions. In the lab I can only generate and measure **real-valued** voltages and **real-valued** voltage functions. Voltage is a **real-valued**, **physical** parameter!*

**A:** You are quite **correct**.

Voltage is a real-valued parameter, expressing electric potential (in Joules) per unit charge (in Coulombs).

**Q:** *So, all your **complex** formulations and **complex** eigen values and **complex** eigen functions may all be sound **mathematical abstractions**, but aren't they **worthless** to us **electrical engineers** who work in the "**real**" world (pun intended)?*

**A:** Absolutely not! Complex analysis actually **simplifies** our analysis of real-valued voltages and currents in **linear circuits** (but **only** for linear circuits!).

The key relationship comes from **Euler's Identity**:

$$e^{j\omega t} = \cos \omega t + j \sin \omega t$$

Meaning:

$$\operatorname{Re}\{e^{j\omega t}\} = \cos \omega t$$



Now, consider a **complex value**  $C$ . We of course can write this complex number in terms of its **real** and **imaginary** parts:

$$C = a + j b \quad \therefore \quad a = \operatorname{Re}\{C\} \quad \text{and} \quad b = \operatorname{Im}\{C\}$$

But, we can **also** write it in terms of its **magnitude**  $|C|$  and **phase**  $\varphi$ !

$$C = |C| e^{j\varphi}$$

where:

$$|C| = C C^* = a^2 + b^2$$

$$\varphi = \tan^{-1} \left[ \frac{b}{a} \right]$$

Thus, the complex **function**  $C e^{j\omega_0 t}$  is:

$$\begin{aligned}
 C e^{j\omega_0 t} &= |C| e^{j\varphi} e^{j\omega_0 t} \\
 &= |C| e^{j\omega_0 t + \varphi} \\
 &= |C| \cos(\omega_0 t + \varphi) + j|C| \sin(\omega_0 t + \varphi)
 \end{aligned}$$

Therefore we find:

$$|C| \cos(\omega_0 t + \varphi) = \operatorname{Re} \{ C e^{j\omega_0 t} \}$$

Now, consider again the **real-valued** voltage function:

$$v_1(t) = V_{m1} \cos(\omega t + \varphi_1)$$

This function is of course **sinusoidal** with a magnitude  $V_{m1}$  and phase  $\varphi_1$ . Using what we have learned above, we can **likewise** express this real function as:

$$\begin{aligned}
 v_1(t) &= V_{m1} \cos(\omega t + \varphi_1) \\
 &= \operatorname{Re} \{ V_1 e^{j\omega t} \}
 \end{aligned}$$

where  $V_1$  is the **complex number**:

$$V_1 = V_{m1} e^{j\varphi_1}$$

**Q:** *I see! A real-valued sinusoid has a magnitude and phase, just like complex number. A single complex number ( $V$ ) can be used to specify both of the fundamental (real-valued) parameters of our sinusoid ( $V_m, \varphi$ ).*

*What I don't see is how this helps us in our circuit analysis.  
After all:*

$$v_2(t) \neq G(\omega_o) \operatorname{Re}\{V_1 e^{j\omega_o t}\}$$

*What then is the **real-valued** output  $v_2(t)$  of our two-port network when the input  $v_1(t)$  is the **real-valued** sinusoid:*

$$\begin{aligned} v_1(t) &= V_{m1} \cos(\omega_o t + \phi_1) \\ &= \operatorname{Re}\{V_1 e^{j\omega_o t}\} \quad ??? \end{aligned}$$

**A:** Let's go back to our **original** convolution integral:

$$v_2(t) = \int_{-\infty}^t g(t-t') v_1(t') dt'$$

If:

$$\begin{aligned} v_1(t) &= V_{m1} \cos(\omega_o t + \phi_1) \\ &= \operatorname{Re}\{V_1 e^{j\omega_o t}\} \end{aligned}$$

then:

$$v_2(t) = \int_{-\infty}^t g(t-t') \operatorname{Re}\{V_1 e^{j\omega_o t'}\} dt'$$

Now, since the impulse function  $g(t)$  is **real-valued** (this is really important!) it can be shown that:

$$\begin{aligned}
 v_2(t) &= \int_{-\infty}^t g(t-t') \operatorname{Re} \{ V_1 e^{j\omega_0 t'} \} dt' \\
 &= \operatorname{Re} \left\{ \int_{-\infty}^t g(t-t') V_1 e^{j\omega_0 t'} dt' \right\}
 \end{aligned}$$

Now, applying what we have **previously** learned:

$$\begin{aligned}
 v_2(t) &= \operatorname{Re} \left\{ \int_{-\infty}^t g(t-t') V_1 e^{j\omega_0 t'} dt' \right\} \\
 &= \operatorname{Re} \left\{ V_1 \int_{-\infty}^t g(t-t') e^{j\omega_0 t'} dt' \right\} \\
 &= \operatorname{Re} \{ V_1 G(\omega_0) e^{j\omega_0 t} \}
 \end{aligned}$$

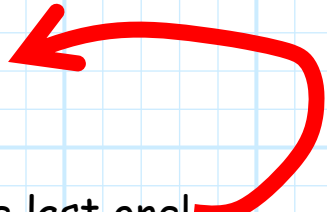
Thus, we **finally** can conclude the real-valued output  $v_2(t)$  due to the **real-valued input**:

$$\begin{aligned}
 v_1(t) &= V_{m1} \cos(\omega_0 t + \phi_1) \\
 &= \operatorname{Re} \{ V_1 e^{j\omega_0 t} \}
 \end{aligned}$$

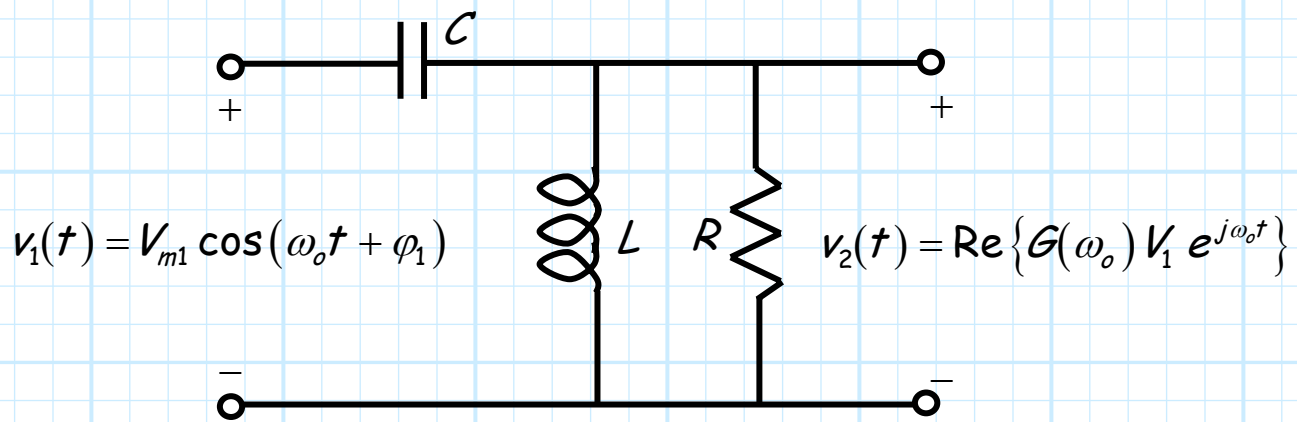
is:

$$\begin{aligned}
 v_2(t) &= \operatorname{Re} \{ V_2 e^{j\omega_0 t} \} \\
 &= V_{m2} \cos(\omega_0 t + \phi_2)
 \end{aligned}$$

where:

$$V_2 = G(\omega_0) V_1$$


The **really important** result here is the last one!



The magnitude and phase of the **output** sinusoid (expressed as **complex** value  $V_2$ ) is related to the magnitude and phase of the **input** sinusoid (expressed as **complex** value  $V_1$ ) by the system **eigen value**  $G(\omega_o)$ :

$$\frac{V_2}{V_1} = G(\omega_o)$$

Therefore we find that **really** often in electrical engineering, we:

1. Use sinusoidal (i.e., eigen function) sources.
2. Express the voltages and currents created by these sources as complex **values** (i.e., **not** as real functions of time)!

For example, we might say " $V_3 = 2.0$ ", meaning:

$$V_3 = 2.0 = 2.0 e^{j0} \Rightarrow v_3(t) = \text{Re}\{2.0 e^{j0} e^{j\omega_o t}\} = 2.0 \cos \omega_o t$$

Or " $I_L = -3.0$ ", meaning:

$$I_L = -2.0 = 3.0 e^{j\pi} \Rightarrow i_L(t) = \text{Re}\{3.0 e^{j\pi} e^{j\omega_0 t}\} = 3.0 \cos(\omega_0 t + \pi)$$

Or " $V_s = j$ ", meaning:

$$V_s = j = 1.0 e^{j(\pi/2)} \Rightarrow v_s(t) = \text{Re}\{1.0 e^{j(\pi/2)} e^{j\omega_0 t}\} = 1.0 \cos(\omega_0 t + \pi/2)$$

- \* Remember, if a linear circuit is excited by a sinusoid (e.g., **eigen function**  $\exp[j\omega_0 t]$ ), then the **only** unknowns are the magnitude and phase of the sinusoidal **currents** and **voltages** associated with **each element** of the circuit.
- \* These unknowns are **completely** described by complex values, as complex values **likewise** have a magnitude and phase.
- \* We can always "**recover**" the **real-valued** voltage or current function by multiplying the complex value by  $\exp[j\omega_0 t]$  and then taking the real part, but typically we don't—after all, **no** new or unknown information is revealed by this operation!

