

# Antenna Directivity

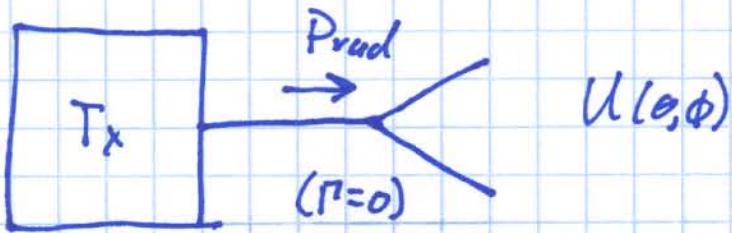
Recall the intensity of the E.M. wave produced by an isotropic radiator (i.e., an antenna that radiates equally in all directions) is

$$U_0 = \frac{P_{\text{rad}}}{4\pi}$$

Remember, an isotropic radiator is actually a physical impossibility — real antennas propagate E.M. energy unequally as a function of direction, a fact represented by the radiation intensity function  $U(\theta, \phi)$ .

Note that  $U(\theta, \phi)$  is dependent on both the antenna and the transmitter power. Increasing the transmitter

power will of course increase  $U(\theta, \phi)$  in all directions.



Of course, this is evident when we consider that the radiated power can be determined from  $U(\theta, \phi)$ :

$$Prad = \int_0^{2\pi} \int_0^{\pi} U(\theta, \phi) \sin \theta d\theta d\phi$$

**Q:** Isn't there some way to characterize the directional behaviour of the antenna only, independent of transmitter power??

**A:** Yes! We call it the antenna directivity pattern  $D(\theta, \phi)$ .

To find a function that describes the antenna behaviour only, we need to somehow normalize  $U(\theta, \phi)$  with respect to  $P_{rad}$ .

We do this by comparing the radiation intensity  $U(\theta, \phi)$  of the antenna to the radiation intensity produced by an isotropic radiator connected to the same transmitter!

I.E.:

$$\begin{aligned}
 D(\theta, \phi) &\doteq \frac{\text{intensity of antenna}}{\text{intensity of an isotropic antenna}} \\
 &= \frac{U(\theta, \phi)}{U_0} \\
 &= \frac{4\pi U(\theta, \phi)}{P_{rad}}
 \end{aligned}$$

Note  $D(\theta, \phi)$  is a unitless value.

We can show that  $D(\theta, \phi)$  is independent of  $P_{\text{rad}}$  by integrating  $D(\theta, \phi)$  over all directions  $\theta$ , and  $\phi$

$$\begin{aligned} & \int_0^{2\pi} \int_0^{\pi} D(\theta, \phi) \sin \theta d\theta d\phi \\ = & \int_0^{2\pi} \int_0^{\pi} \frac{4\pi U(\theta, \phi)}{P_{\text{rad}}} \sin \theta d\theta d\phi \\ = & \frac{4\pi}{P_{\text{rad}}} \int_0^{2\pi} \int_0^{\pi} U(\theta, \phi) \sin \theta d\theta d\phi \\ = & \frac{4\pi}{P_{\text{rad}}} (P_{\text{rad}}) \\ = & \underline{\underline{\frac{4\pi}{P_{\text{rad}}}}} \end{aligned}$$

$$\boxed{\int_0^{2\pi} \int_0^{\pi} D(\theta, \phi) \sin \theta d\theta d\phi = 4\pi}$$

Furthermore, we find that the average value of  $D(\theta, \phi)$  across  $4\pi$  steradians (i.e., across all directions  $\theta, \phi$ ) is:

$$D_{ave} = \frac{1}{4\pi} \iint_0^{2\pi} D(\theta, \phi) \sin\theta d\theta d\phi$$

$$= \frac{1}{4\pi} (4\pi) = \underline{\underline{1}}$$

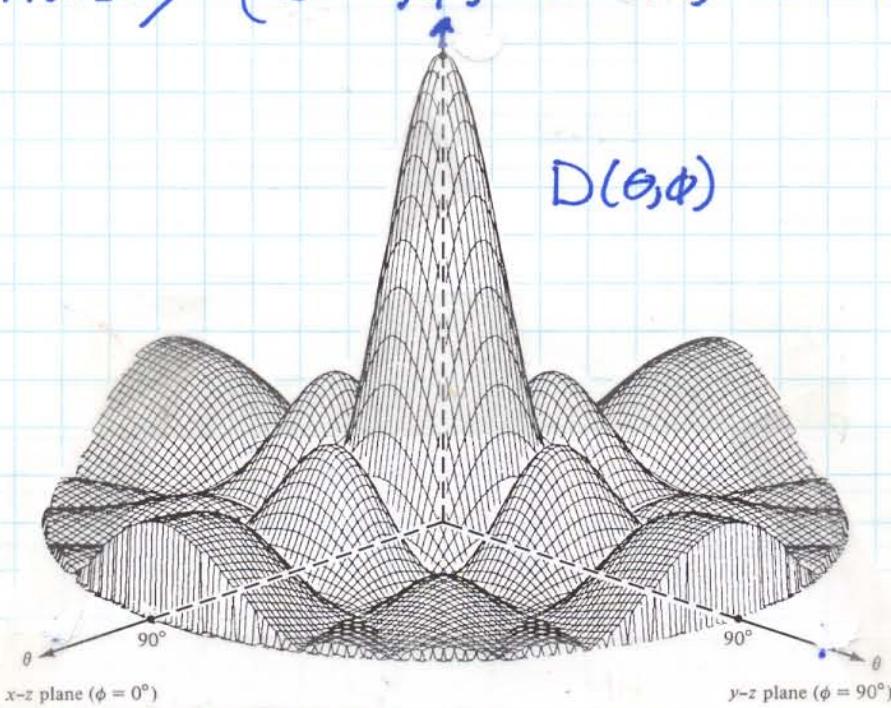
In other words, the average value of  $D(\theta, \phi)$ , across all directions  $\theta, \phi$ , of any and all antennas is 1!

What this means is that an antenna may produce an intensity larger than that of an isotropic radiator ( $I_0$ ) in some directions, but then it must produce an intensity less than an isotropic radiator in other directions.

Likewise, if the intensity is much, much larger than  $I_0$  in a specific direction, then the intensity must be very small in many other directions.

$\Rightarrow$  In other words, the antenna cannot produce above average intensity in all directions !!

Typically, an antenna will produce very large intensity (i.e.,  $D(\theta, \phi) \gg 1$ ) in one general direction, and very small intensity ( $D(\theta, \phi) \ll 1$ ) in the rest.



Note that there will typically be one direction where the function  $D(\theta, \phi)$  is its maximum value.

This maximum value is defined as the antennas directivity:

$$\text{Directivity} \doteq D_0 = D(\theta, \phi) \Big|_{\max}$$

Note  $D_0$  is a number (often expressed in dB) while directivity pattern  $D(\theta, \phi)$  is a function of  $\theta$  and  $\phi$ .