

The Chebyshev Matching Transformer

An **alternative** to Binomial (Maximally Flat) functions (and there are **many** such alternatives!) are **Chebyshev** polynomials.



**Pafnuty
Chebyshev**

1821 -1894

Chebyshev solutions can provide functions $\Gamma(\omega)$ with **wider bandwidth** than the Binomial case—albeit at the “expense” of **passband ripple**.

It is evident from the plot below that the Chebyshev response is **far** from maximally flat! Instead, a Chebyshev matching network exhibits a “**ripple**” in its passband. Note the magnitude of this ripple never exceeds some **maximum** value Γ_m (within the **pass-band**).

The two frequencies at which the value $|\Gamma(\omega)|$ **does** increase beyond Γ_m define the **bandwidth** of the matching network.

We denote these frequencies $\omega_m = 2\pi f_m$ (the plot above shows the locations of the frequencies for $N = 4$).

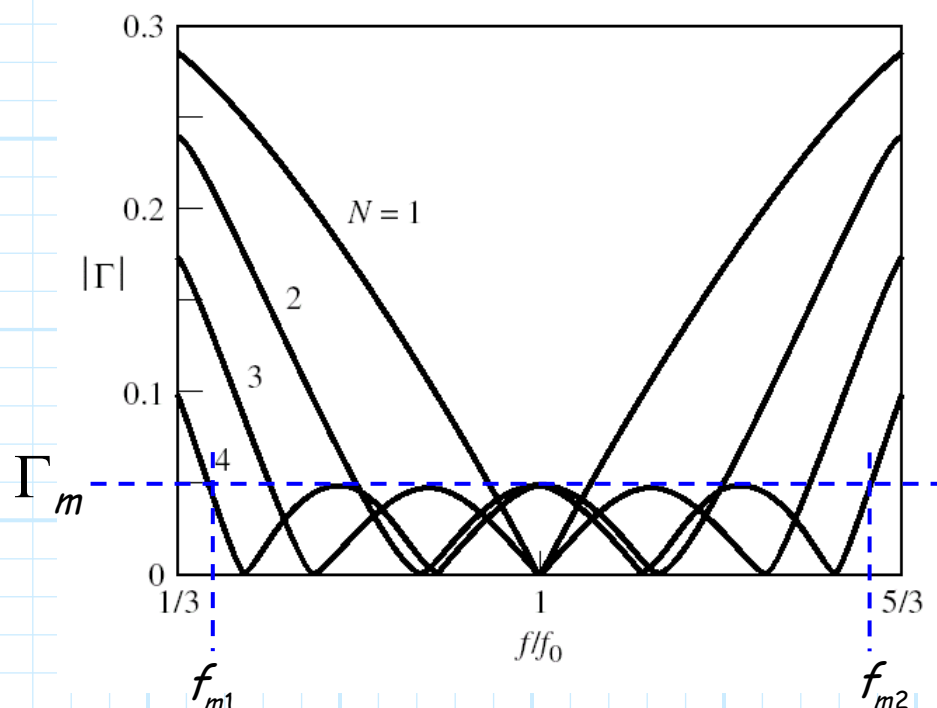


Figure 5.17 (p. 255)

Reflection coefficient magnitude versus frequency for the Chebyshev multisection matching transformers of Example 5.7.

→ Note that the **bandwidth** defined by f_m **increases** as the **number of sections N** is increased.

→ Note also that the reflection coefficient is **not necessarily zero** at the design frequency f_0 !!!

Instead, we find:

$$|\Gamma(f = f_0)| = \begin{cases} 0 & \text{for odd-valued } N \\ \Gamma_m & \text{for even-valued } N \end{cases}$$

Now, Chebyshev transformers are **symmetric**, i.e.:

$$\Gamma_0 = \Gamma_N, \quad \Gamma_1 = \Gamma_{N-1}, \text{ etc.}$$

Recall we can express the multi-section function $\Gamma(\theta)$ (where $\theta = \omega T = \beta l$) in a **simpler form** when the transformer is symmetric:

$$\Gamma(\theta) = 2 e^{-jN\theta} \left[\Gamma_0 \cos N\theta + \Gamma_1 \cos(N-2)\theta + \dots + \Gamma_n \cos(N-2n)\theta + \dots + G(\theta) \right]$$

where:

$$G(\theta) = \begin{cases} \frac{1}{2} \Gamma_{N/2} & \text{for } N \text{ even} \\ \Gamma_{(N-1)/2} \cos \theta & \text{for } N \text{ odd} \end{cases}$$

Now, the reflection coefficient of a **Chebyshev** matching network has the form:

$$\begin{aligned} \Gamma(\theta) &= A e^{-jN\theta} T_N \left(\frac{\cos \theta}{\cos \theta_m} \right) \\ &= A e^{-jN\theta} T_N (\cos \theta \sec \theta_m) \end{aligned}$$

where $\theta_m = \omega_m T$

The function $T_N(\cos \theta \sec \theta_m)$ is a **Chebyshev polynomial** of order N .

$$T_1(x) = x$$

$$T_2(x) = 2x^2 - 1$$

$$T_3(x) = 4x^3 - 3x$$

$$T_4(x) = 8x^4 - 8x^2 + 1$$

We can determine **higher-order** Chebyshev polynomials using the **recursive formula**:

$$T_n(x) = 2x T_{n-1}(x) - T_{n-2}(x)$$

Inserting the **substitution**:

$$x = \cos \theta \sec \theta_m$$

into the Chebyshev polynomials above (and then applying a few **trig identities**) gives the results shown in equations 5.60 on page 252 of **your** book:

$$T_1(\cos \theta \sec \theta_m) = \cos \theta \sec \theta_m$$

$$\begin{aligned} T_2(\cos \theta \sec \theta_m) &= \sec^2 \theta_m (1 + \cos 2\theta) - 1 \\ &= \sec^2 \theta_m \cos 2\theta + (\sec^2 \theta_m - 1) \end{aligned}$$

$$\begin{aligned} T_3(\cos \theta \sec \theta_m) &= \sec^3 \theta_m (\cos 3\theta + 3 \cos \theta) - 3 \sec \theta_m \cos \theta \\ &= \sec^3 \theta_m \cos 3\theta + (3 \sec^2 \theta_m - 3) \sec \theta_m \cos \theta \end{aligned}$$

$$\begin{aligned} T_4(\cos \theta \sec \theta_m) &= \sec^4 \theta_m (\cos 4\theta + 4 \cos 2\theta + 3) \\ &\quad - 4 \sec^2 \theta_m (\cos 2\theta + 1) + 1 \\ &= \sec^4 \theta_m \cos 4\theta \\ &\quad + 4 \sec^2 \theta_m (\sec^2 \theta_m - 1) \cos 2\theta \\ &\quad + (3 \sec^4 \theta_m - 4 \sec^2 \theta_m + 1) \end{aligned}$$

Note that these polynomials have a $\cos N\theta$ term, a $\cos(N-2)\theta$ term, $\cos(N-4)\theta$ term, etc.—**just** like the **symmetric** multi-section transformer function!

For example, a 4-section **Chebyshev** matching network will have the form:

$$\begin{aligned} \Gamma(\theta) &= A e^{-j4\theta} T_4(\cos \theta \sec \theta_m) \\ &= A e^{-j4\theta} \left[\sec^4 \theta_m \cos 4\theta \right. \\ &\quad + 4 \sec^2 \theta_m (\sec^2 \theta_m - 1) \cos 2\theta \\ &\quad \left. + (3 \sec^4 \theta_m - 4 \sec^2 \theta_m + 1) \right] \end{aligned}$$

While the **general form** of a 4-section matching transformer is a polynomial with these **same** terms:

$$\begin{aligned}
 \Gamma_4(\theta) &= 2 e^{-jN\theta} \left[\Gamma_0 \cos N\theta + \Gamma_1 \cos(N-2)\theta + \frac{1}{2} \Gamma_2 \right] \Big|_{N=4} \\
 &= 2 e^{-j4\theta} \left[\Gamma_0 \cos 4\theta + \Gamma_1 \cos(4-2)\theta + \frac{1}{2} \Gamma_2 \right] \\
 &= 2 e^{-j4\theta} \left[\Gamma_0 \cos 4\theta + \Gamma_1 \cos 2\theta + \frac{1}{2} \Gamma_2 \right]
 \end{aligned}$$

Thus, we can **determine** the values of marginal reflection coefficients $\Gamma_0, \Gamma_1, \Gamma_2$ by simply **equating** the **3 terms** of the two previous expressions:

$$\begin{aligned}
 2 e^{-j4\theta} \Gamma_0 \cos 4\theta &= A e^{-j4\theta} \sec^4 \theta_m \cos 4\theta \\
 \Rightarrow \Gamma_0 &= \frac{1}{2} A \sec^4 \theta_m
 \end{aligned}$$

$$\begin{aligned}
 2 e^{-j4\theta} \Gamma_1 \cos 2\theta &= A e^{-j4\theta} 4 \sec^2 \theta_m (\sec^2 \theta_m - 1) \cos 2\theta \\
 \Rightarrow \Gamma_1 &= A 2 \sec^2 \theta_m (\sec^2 \theta_m - 1)
 \end{aligned}$$

$$\begin{aligned}
 2 e^{-j4\theta} \frac{1}{2} \Gamma_2 &= A e^{-j4\theta} (3 \sec^4 \theta_m - 4 \sec^2 \theta_m + 1) \\
 \Rightarrow \Gamma_2 &= A (3 \sec^4 \theta_m - 4 \sec^2 \theta_m + 1)
 \end{aligned}$$

And because it's **symmetric**, we also know that $\Gamma_3 = \Gamma_1$ and $\Gamma_4 = \Gamma_0$.

Now, we can **again** (i.e., as we did in the binomial matching network) determine the values of characteristic impedance Z_n , using the **iterative** (approximate) relationship:

$$Z_{n+1} = Z_n \exp[2\Gamma_n]$$

Q: *But what about the value of A ?*

A: Also using the same **boundary condition** analysis that we used for the binomial function, we find from our **transmission line** knowledge that for **any** multi-section matching network, at $\theta = 0$:

$$\Gamma(\theta = 0) = \frac{R_L - Z_0}{R_L + Z_0}$$

Likewise, a **Chebyshev** matching network will have the specific value at $\theta = 0$ of:

$$\begin{aligned} \Gamma(\theta = 0) &= A e^{-jN(0)} T_N(\sec \theta_m \cos(0)) \\ &= A T_N(\sec \theta_m) \end{aligned}$$


These two results must of course be **equal**, and equating them allows us to solve for A :

$$A = \frac{R_L - Z_0}{R_L + Z_0} \frac{1}{T_N(\sec \theta_m)}$$

Here again (just like the binomial case) we will find it advantageous to use the approximation:

$$\frac{R_L - Z_0}{R_L + Z_0} \approx \frac{1}{2} \ln \left(\frac{R_L}{Z_0} \right)$$

So that the value A is **approximately**:

$$A \approx \frac{1}{2} \frac{\ln(R_L/Z_0)}{T_N(\sec \theta_m)} \quad (A \text{ can be negative!})$$


Q: Gosh, both the values of marginal reflection coefficients Γ_n and value A depend explicitly on $\sec \theta_m$. Just what is this value, and how do we determine it?

A: Recall that $\theta_m = \omega_m T$, where T is the propagation time through one section (i.e., $T = \ell/v_p$) and $\omega_m = 2\pi f_m$ defines the bandwidth associated with ripple value Γ_m . Thus, for a given ripple Γ_m and value N , we can find $\sec \theta_m$ by solving this equations

$$\begin{aligned} \Gamma_m &= |\Gamma(\theta = \theta_m)| \\ &= |A e^{-jN\theta_m} T_N(\sec \theta_m \cos \theta_m)| \\ &= |A| |e^{-jN\theta_m}| |T_N(\sec \theta_m \cos \theta_m)| \\ &= |A| |T_N(1)| \end{aligned}$$

Q: *Yikes! The value $\sec \theta_m$ disappeared from this equation; how can we use this to determine $\sec \theta_m$?*

A: Don't forget the value A !! Inserting this into the expression:

$$\begin{aligned}\Gamma_m &= \left| \Gamma(\theta = \theta_m) \right| \\ &= |A| \left| T_N(1) \right| \\ &= \frac{1}{2} \frac{\left| \ln(R_L/Z_0) \right|}{\left| T_N(\sec \theta_m) \right|} \left| T_N(1) \right|\end{aligned}$$

One **property** of Chebyshev polynomials is that:

$$\left| T_N(1) \right| = 1 \quad \text{for all values } N$$

Therefore, we **conclude**:

$$\Gamma_m = \left| \Gamma(\theta = \theta_m) \right| = \frac{1}{2} \frac{\left| \ln(R_L/Z_0) \right|}{\left| T_N(\sec \theta_m) \right|}$$

And so rearranging:

$$\left| T_N(\sec \theta_m) \right| = \frac{1}{2\Gamma_m} \left| \ln(R_L/Z_0) \right|$$

Note that R_L, Z_0 and Γ_m are design parameters, thus we can use the above to determine $\left| T_N(\sec \theta_m) \right|$, and thus $\sec \theta_m$!!!

Q: Um, I'm not at all clear about how one determines $\sec \theta_m$ from the value $|T_N(\sec \theta_m)|$. Can you be more specific??

A: Perhaps I should.

Recall that the Chebyshev polynomials we use in the design of this matching transformer were of the form $T_N(\cos \theta \sec \theta_m)$, i.e.:

$$\Gamma(\theta) = A e^{-jN\theta} T_N(\cos \theta \sec \theta_m)$$

Note the value $|T_N(\sec \theta_m)|$ is just the magnitude of the Chebyshev $T_N(\cos \theta \sec \theta_m)$ when evaluated at $\cos \theta = 1$, which is the case when $\theta = 0$!!

$$|T_N(\cos \theta \sec \theta_m)|_{\theta=0} = |T_N(\cos 0 \sec \theta_m)| = |T_N(\sec \theta_m)|$$



Now, it can be shown that (← a phrase professors use while in hand-waving mode!) for all values θ outside the passband of the matching network, the general form of the Chebyshev polynomial can also be written as:

$$T_N(\sec \theta_m \cos \theta) = \cosh \left[N \cosh^{-1}(\sec \theta_m \cos \theta) \right]$$

Note the value $\theta = 0 = \omega T$ means that the frequency $\omega = 0$. This frequency is most definitely **outside** the passband, and thus according to the **above** expression:

$$T_N(\sec \theta_m \cos(\theta = 0)) = T_N(\sec \theta_m) \\ = \cosh[N \cosh^{-1}(\sec \theta_m)]$$

Likewise,

Q: I know I *should* remember exactly what function **cosh** is, but I don't. Can you help *refresh* my memory?

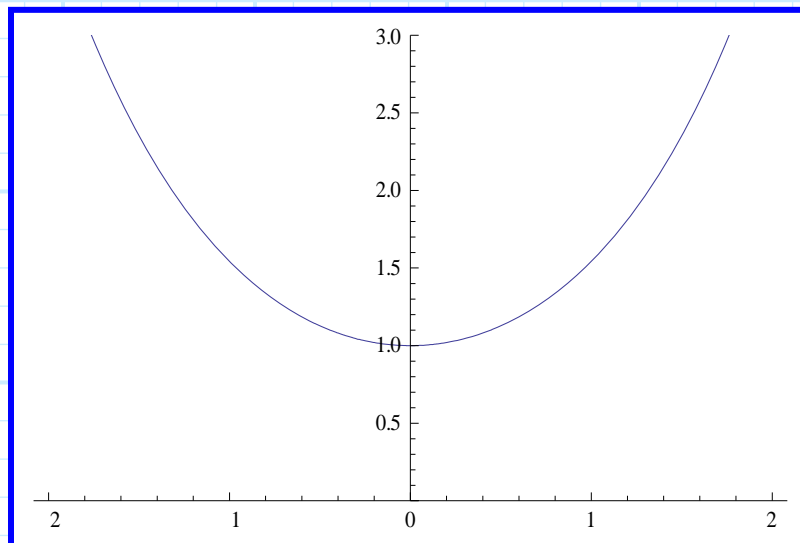
A: The function *cosh* is the **hyperbolic cosine**. Recall that **cosine** (the "regular" kind) can be expressed as:

$$\cos \theta = \frac{e^{j\theta} + e^{-j\theta}}{2}$$

Similarly, the **hyperbolic cosine** is:

$$\cosh x = \frac{e^x + e^{-x}}{2}$$

Plotting $\cosh x$ from $x = -2$ to $x = +2$:



Hopefully it is apparent to **you**, from the above expression for $\cosh x$, that it results in a real value that is always greater than or equal to one (provided x is real):

$$\cosh x \geq 1 \quad \text{for } -\infty < x < \infty$$

Thus $|\cosh x| = \cosh x$.

Q: What about $\cosh^{-1}y$?

A: The function $\cosh^{-1}y$ is the **inverse** hyperbolic cosine, **aka** the hyperbolic **arccosine** ($\text{arcosh } y$). Note that this value is defined only for $y \geq 1$, and is specifically:

$$\cosh^{-1}y = \pm \ln\left(y + \sqrt{y^2 - 1}\right) \quad \text{for } y \geq 1$$

Note that there is always **two solutions** (positive and negative) for the inverse hyperbolic cosine!

You will find that most scientific **calculators** support the \cosh and \cosh^{-1} functions as well.

Anyway, combining the previous results, we find:

$$\left|T_N(\sec \theta_m)\right| = \frac{1}{2\Gamma_m} \left| \ln \frac{R_L}{Z_0} \right| = \left| \cosh \left[N \cosh^{-1}(\sec \theta_m) \right] \right|$$

Therefore:

$$\frac{1}{2\Gamma_m} \left| \ln \frac{R_L}{Z_0} \right| = \cosh \left[N \cosh^{-1} (\sec \theta_m) \right]$$

Now (finally!) we have a form that can be manipulated algebraically. Solving the above equation for $\sec \theta_m$:

$$\sec \theta_m = \pm \cosh \left[\frac{1}{N} \cosh^{-1} \left(\frac{1}{2\Gamma_m} \left| \ln \frac{R_L}{Z_0} \right| \right) \right]$$

Of course, the specific values of θ_m can be determined with the \sec^{-1} (i.e., arcsecant) function.

Note there are two solutions for \sec^{-1} (one for the plus sign and one for the minus): The two solutions are related as:

$$\theta_1 = \pi - \theta_2$$

Now, we can convert the values of θ_m into specific bandwidth frequencies f_{m1} and f_{m2} .

Since $\theta = \omega T$, we find:

$$\omega_{m1} = \frac{1}{T} \theta_m = \frac{v_p}{\ell} \theta_1$$

And similarly:

$$\omega_{m2} = \frac{1}{T} \theta_m = \frac{v_p}{\ell} \theta_2$$

Note that there are **two** solutions θ_m for this equation—one value of θ_m (θ_1) will be **less** than $\pi/2$ (defining the **lower** passband frequency), while the **other** (θ_2) will be **greater** than $\pi/2$ (defining the **upper** passband frequency).

Moreover, we find that the **two** values of θ_m will be **symmetric** about the value $\pi/2$! For example, if the **lower** value θ_1 is $\pi/2 - \pi/10$, then the **upper** value θ_2 will be $\pi/2 + \pi/10$.

Q: So??

A: This means that the **center** of the passband will be defined by the value $\theta = \pi/2$ —and the center of the passband is our **design frequency** ω_0 ! In other words, since $\omega_0 T = \pi/2$:

$$\omega_0 = \frac{\pi}{2} \frac{1}{T} = \frac{\pi}{2} \frac{v_p}{\ell}$$

Thus, we set the center (i.e., design) frequency by **selecting** the proper value of **section length** ℓ . Note the above expression is **precisely** the same result obtained for the **Binomial** matching network, and thus we have precisely the **same** design rule!

That **design rule** is, set the section lengths ℓ such that they are a **quarter wavelength** at the **design frequency** ω_0 :

$$\ell = \frac{\lambda_0}{4}$$

where $\lambda_0 = v_p / \omega_0$.

Summarizing, the Chebyshev matching network design procedure is:

1. Determine the value N required to meet the bandwidth and ripple Γ_m requirements.

2. Determine the Chebyshev function

$$\Gamma(\theta) = A e^{-jN\theta} T_N(\cos \theta \sec \theta_m).$$

3. Determine all Γ_n by equating terms with the symmetric multisection transformer expression:

$$\Gamma(\theta) = 2 e^{-jN\theta} [\Gamma_0 \cos N\theta + \Gamma_1 \cos(N-2)\theta + \dots + \Gamma_n \cos(N-2n)\theta + \dots + G(\theta)]$$

4. Calculate all Z_n using the approximation:

$$\Gamma_n = \frac{1}{2} \ln \frac{Z_{n+1}}{Z_n}$$

5. Determine section length $\ell = \lambda_0 / 4$.