

# The $\lambda/4$ Transformer- Yet Again

Let's go back and again look at the quarter wave transformer.

This time we will look at it more **critically**, and discover that this matching network has a few **problems**!

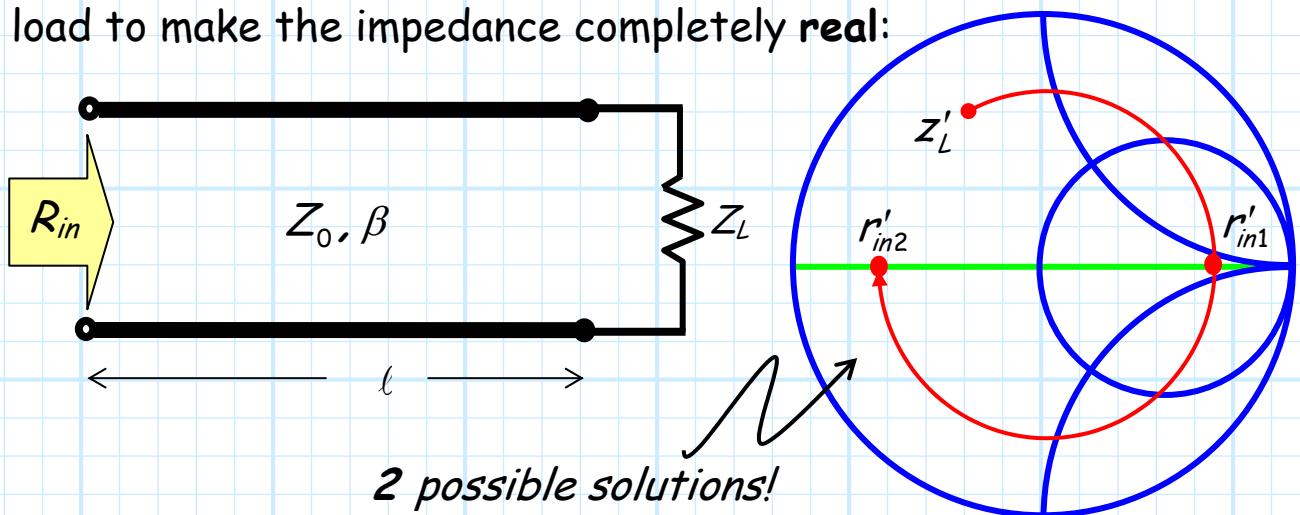
## Problem #1

Recall the matching solution was limited to loads that were **purely real!** I.E.:

$$Z_L = R_L + j0$$

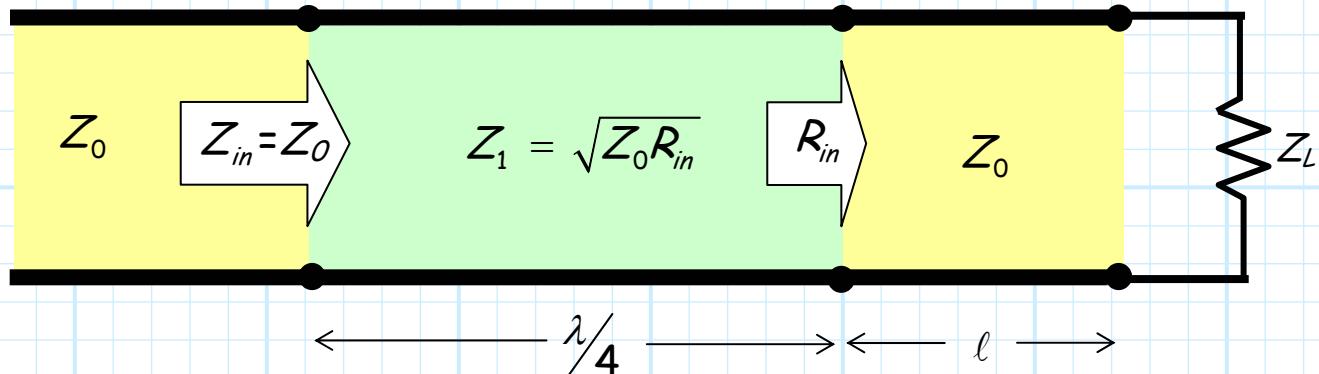
Of course, this is a **BIG** problem, as most loads will have a **reactive** component!

Fortunately, we have a relatively easy **solution** to this problem, as we can always add some **length**  $\ell$  of transmission line to the load to make the impedance completely **real**:



However, remember that the input impedance will be purely real at only **one** frequency!

We can then build a quarter-wave transformer to **match** the line  $Z_0$  to resistance  $R_{in}$ :



Again, since the transmission lines are lossless, **all** of the incident power is delivered to the **load**  $Z_L$ .

### Problem #2

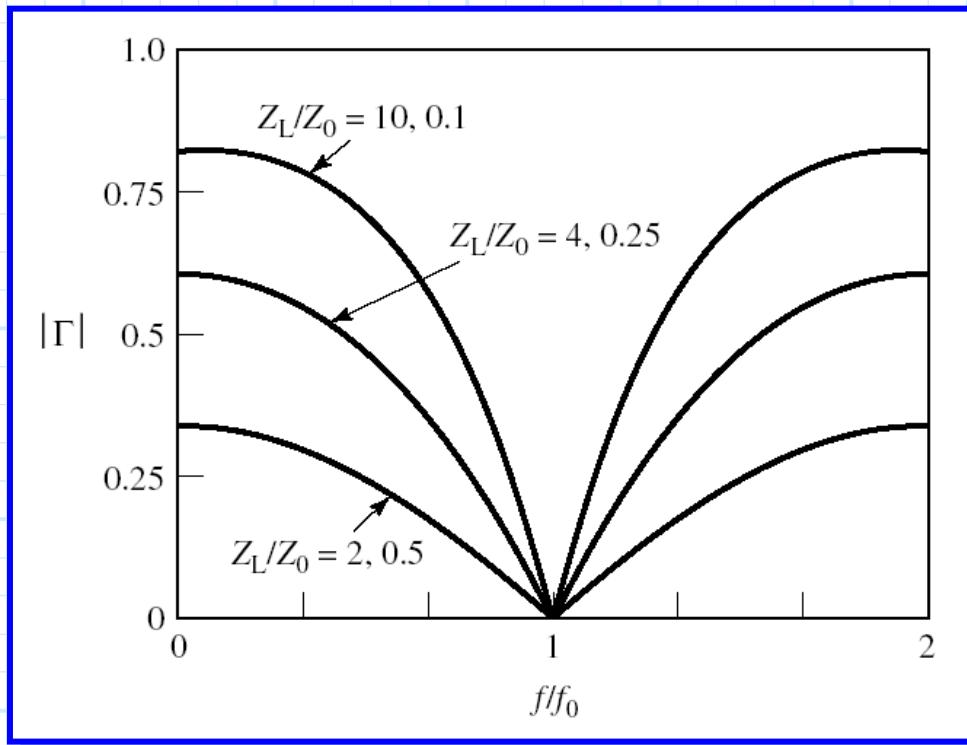
The matching bandwidth is **narrow**!

In other words, we obtain a **perfect** match at precisely the frequency where the length of the matching transmission line is a **quarter-wavelength**.

→ But remember, this length can be a quarter-wavelength at just **one** frequency!

As the signal frequency (i.e., wavelength) changes, the **electrical** length of the matching transmission line changes. It will no longer be a quarter wavelength, and thus we no longer will have a **perfect** match.

We find that the closer  $R_L$  ( $R_{in}$ ) is to characteristic impedance  $Z_0$ , the wider the bandwidth of the quarter wavelength transformer.



**Figure 5.12 (p. 243)** Reflection coefficient magnitude versus frequency for a single-section quarter-wave matching transformer with various load mismatches.

We will find that the bandwidth can be increased by adding multiple  $\lambda/4$  sections!