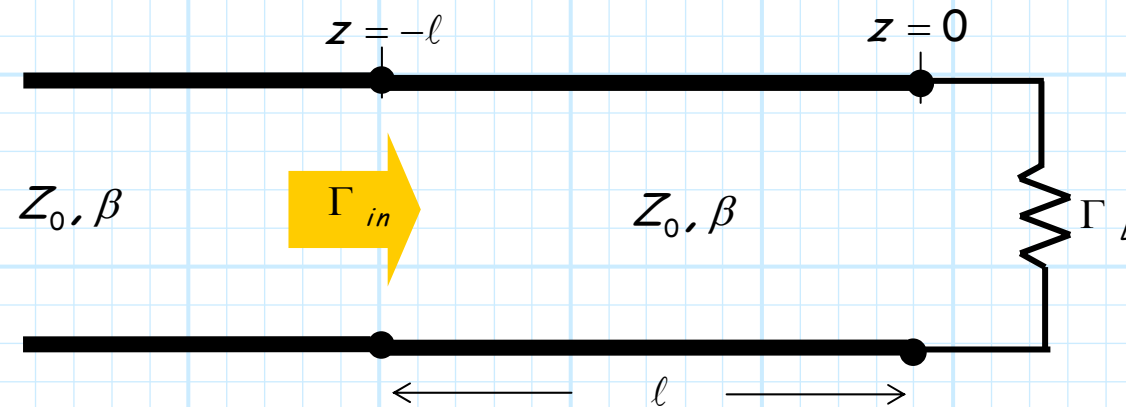


# Transformations on the Complex $\Gamma$ Plane

The usefulness of the complex  $\Gamma$  plane is apparent when we consider again the **terminated, lossless transmission line**:



Recall that the reflection coefficient function for **any** location  $z$  along the transmission line can be expressed as (since  $z_L = 0$ ):

$$\Gamma(z) = \Gamma_L e^{j2\beta z} = |\Gamma_L| e^{j(\theta_r + 2\beta z)}$$

And thus, as we would **expect**:

$$\Gamma(z = 0) = \Gamma_L \quad \text{and} \quad \Gamma(z = -l) = \Gamma_L e^{-j2\beta l} = \Gamma_{in}$$

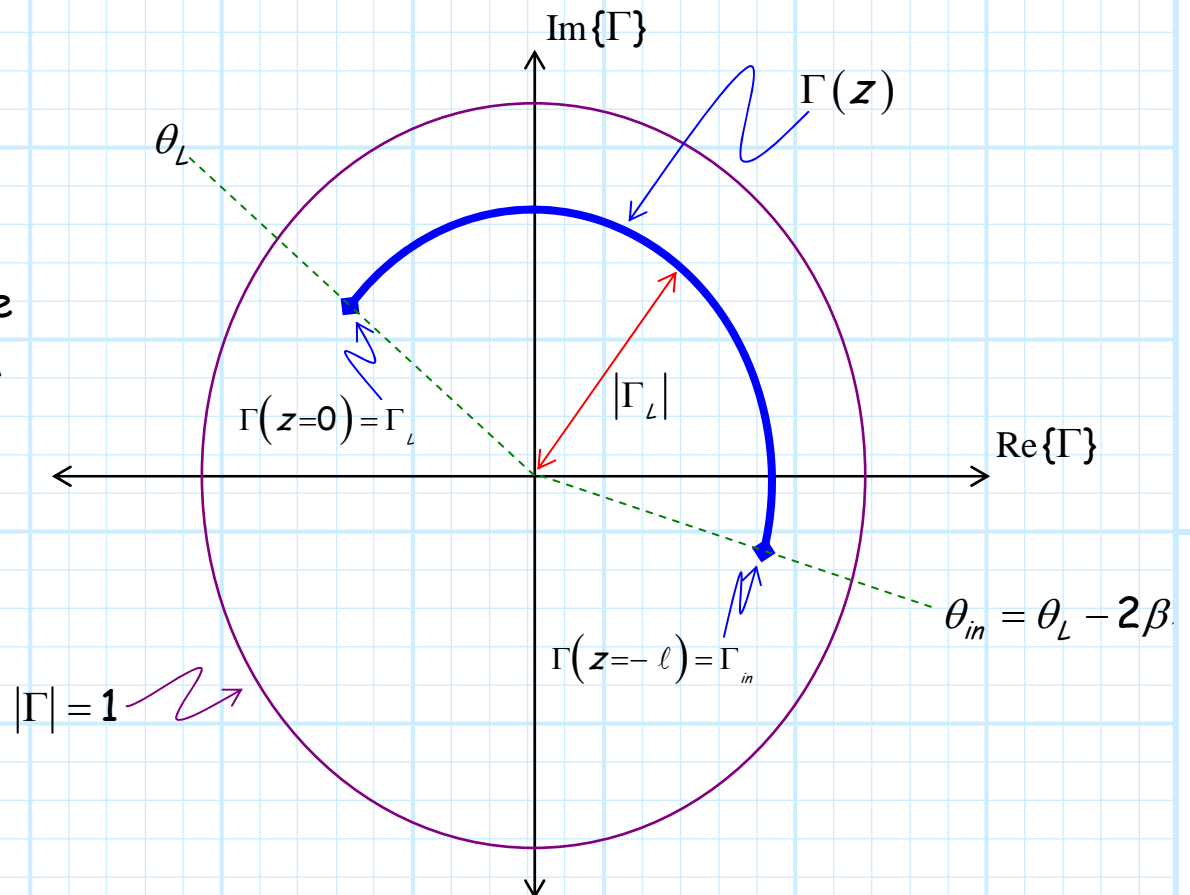
## Transforming $\Gamma_L$ to $\Gamma_{in}$

Recall this result "says" that adding a transmission line of length  $\ell$  to a load results in a **phase shift** in  $\theta_r$  by  $-2\beta\ell$  radians, while the **magnitude**  $|\Gamma|$  remains **unchanged**.



**Q:** Magnitude  $|\Gamma|$  and phase  $\theta_r$  --aren't those the values used when plotting on the complex  $\Gamma$  plane?

**A:** Precisely! In fact, plotting the transformation of  $\Gamma_L$  to  $\Gamma_{in}$  along a transmission line length  $\ell$  has an interesting **graphical** interpretation. Let's **parametrically** plot  $\Gamma(z)$  from  $z = z_L$  (i.e.,  $z = 0$ ) to  $z = z_L - \ell$  (i.e.,  $z = -\ell$ ):



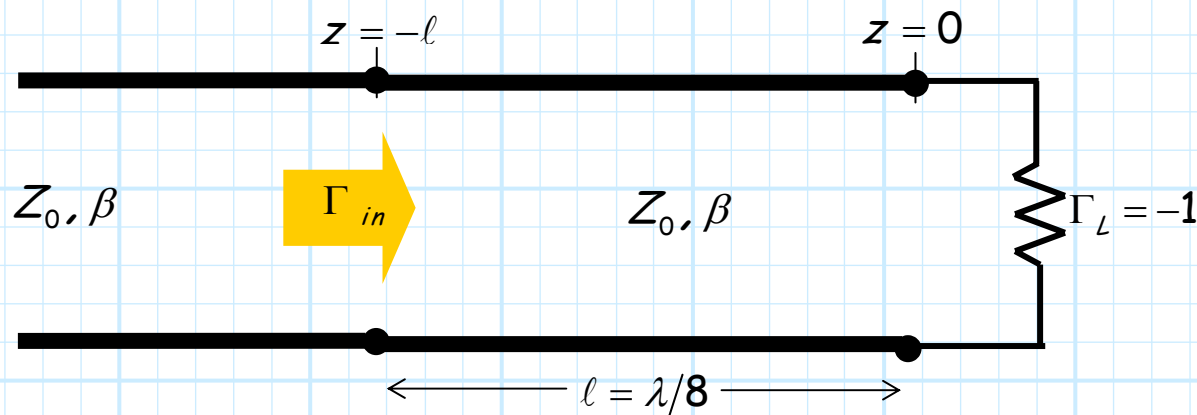
## Graphically Transforming $\Gamma_L$ to $\Gamma_{in}$



Since adding a length of transmission line to a load  $\Gamma_L$  **modifies** the **phase**  $\theta_r$  but **not** the **magnitude**  $|\Gamma_L|$ , we trace a **circular arc** as we parametrically plot  $\Gamma(z)$ ! This arc has a **radius**  $|\Gamma_L|$  and an **arc angle**  $2\beta\ell$  radians.

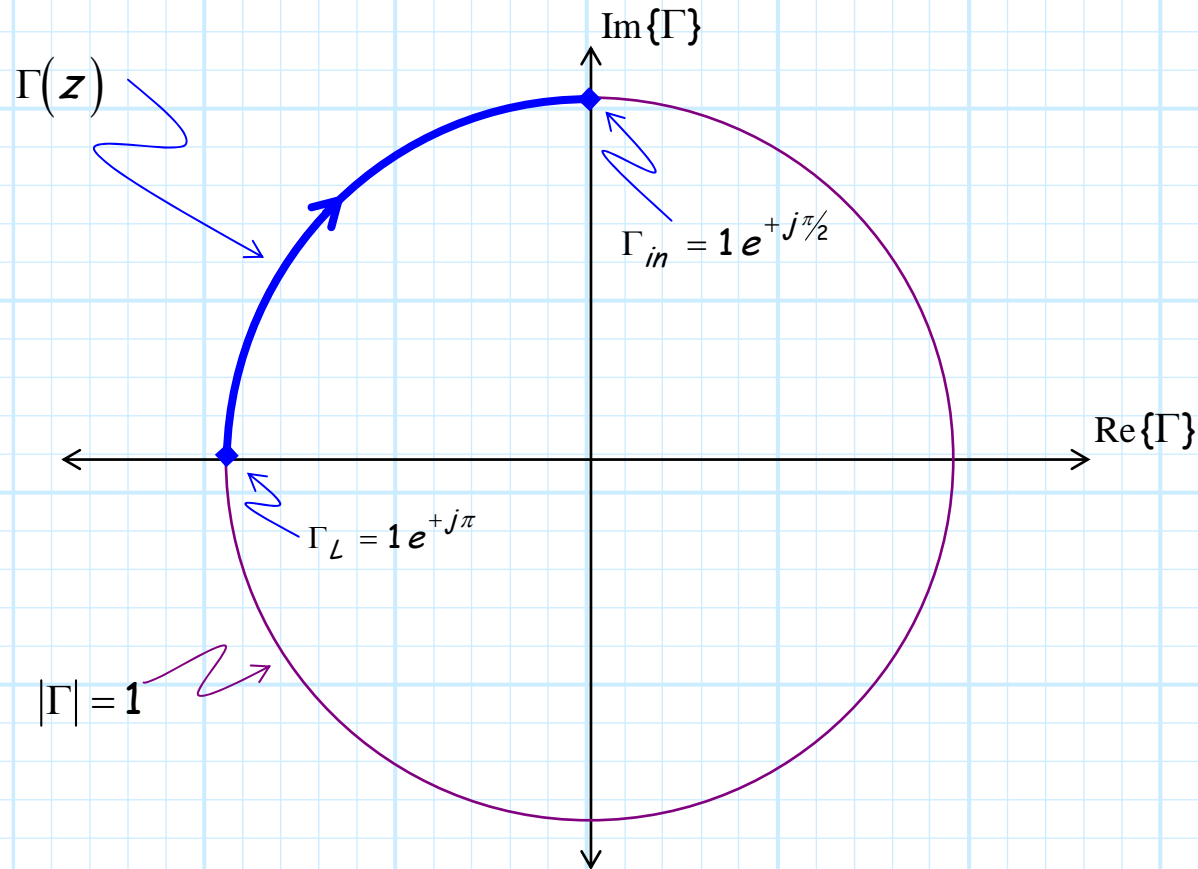
With this knowledge, we can **easily** solve many interesting transmission line problems **graphically**—using the complex  $\Gamma$  plane!

For **example**, say we wish to determine  $\Gamma_{in}$  for a transmission line length  $\ell = \lambda/8$  and terminated with a **short** circuit.



## Example: Graphically Transforming $\Gamma_L$ to $\Gamma_{in}$

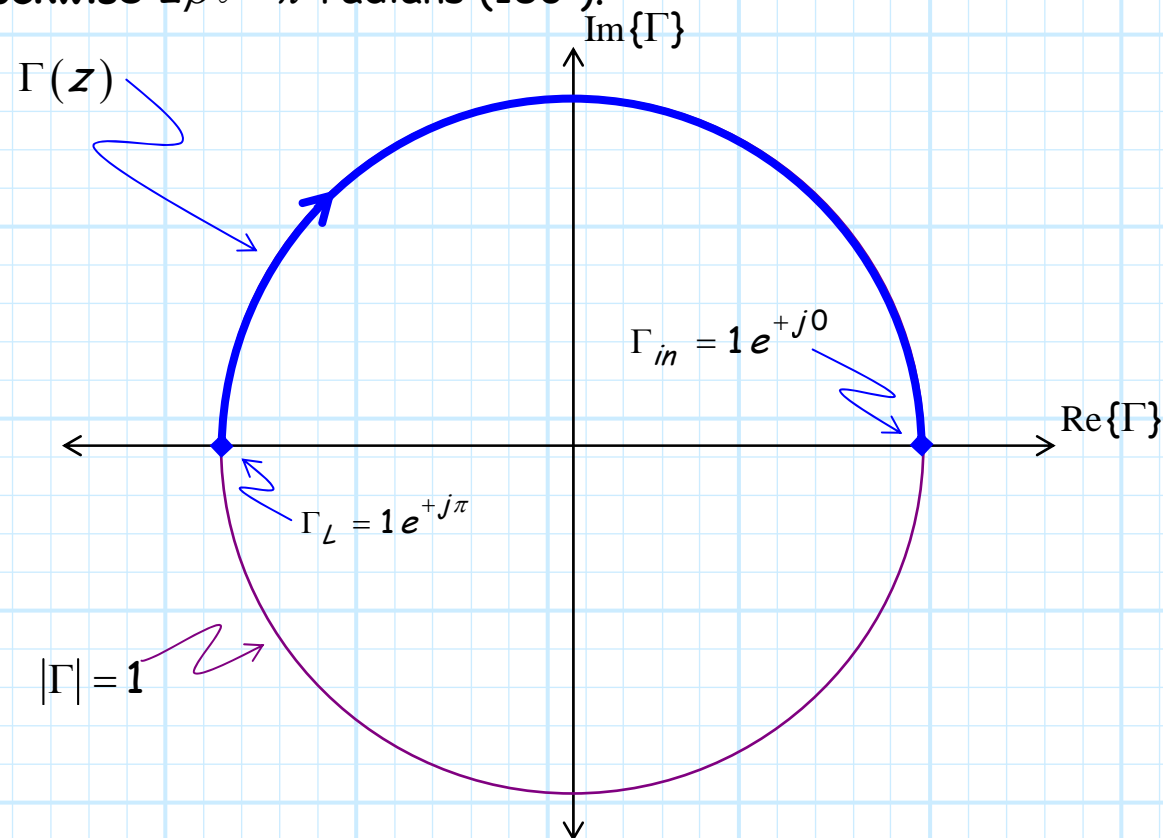
The reflection coefficient of a **short circuit** is  $\Gamma_L = -1 = 1 e^{j\pi}$ , and therefore we **begin** at that point on the complex  $\Gamma$  plane. We then move along a **circular arc**  $-2\beta l = -2(\pi/4) = -\pi/2$  radians (i.e., rotate **clockwise**  $90^\circ$ ).



When we **stop**, we find we are at the point for  $\Gamma_{in}$ ; in this case  $\Gamma_{in} = 1e^{j\pi/2}$  (i.e., magnitude is **one**, phase is  $90^\circ$ ).

## Example: Now with $\ell = \lambda/4$

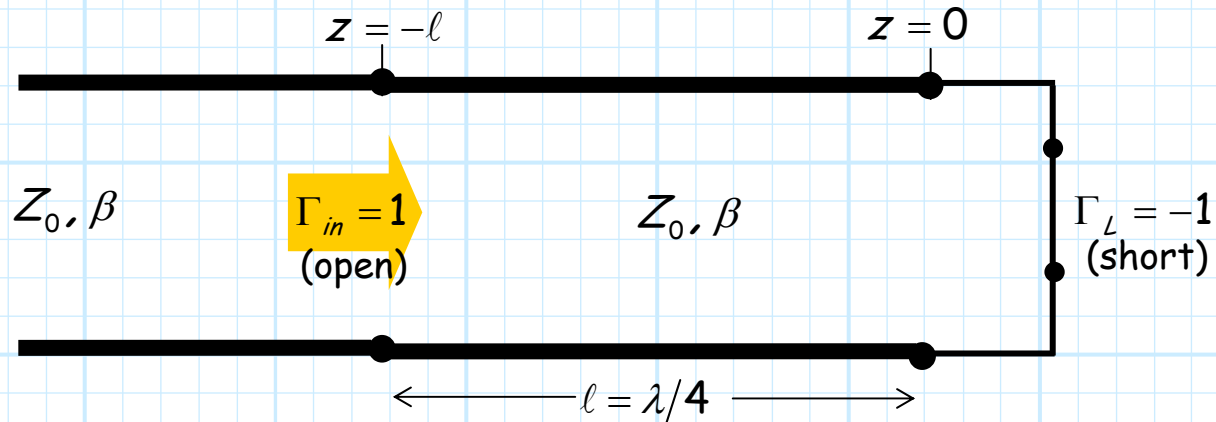
Now, let's **repeat** this same problem, only with a **new** transmission line length of  $\ell = \lambda/4$ .  
 Now we rotate **clockwise**  $2\beta\ell = \pi$  radians ( $180^\circ$ ).



For this case, the **input** reflection coefficient is  $\Gamma_{in} = 1e^{j0} = 1$  : the reflection coefficient of an **open circuit!**

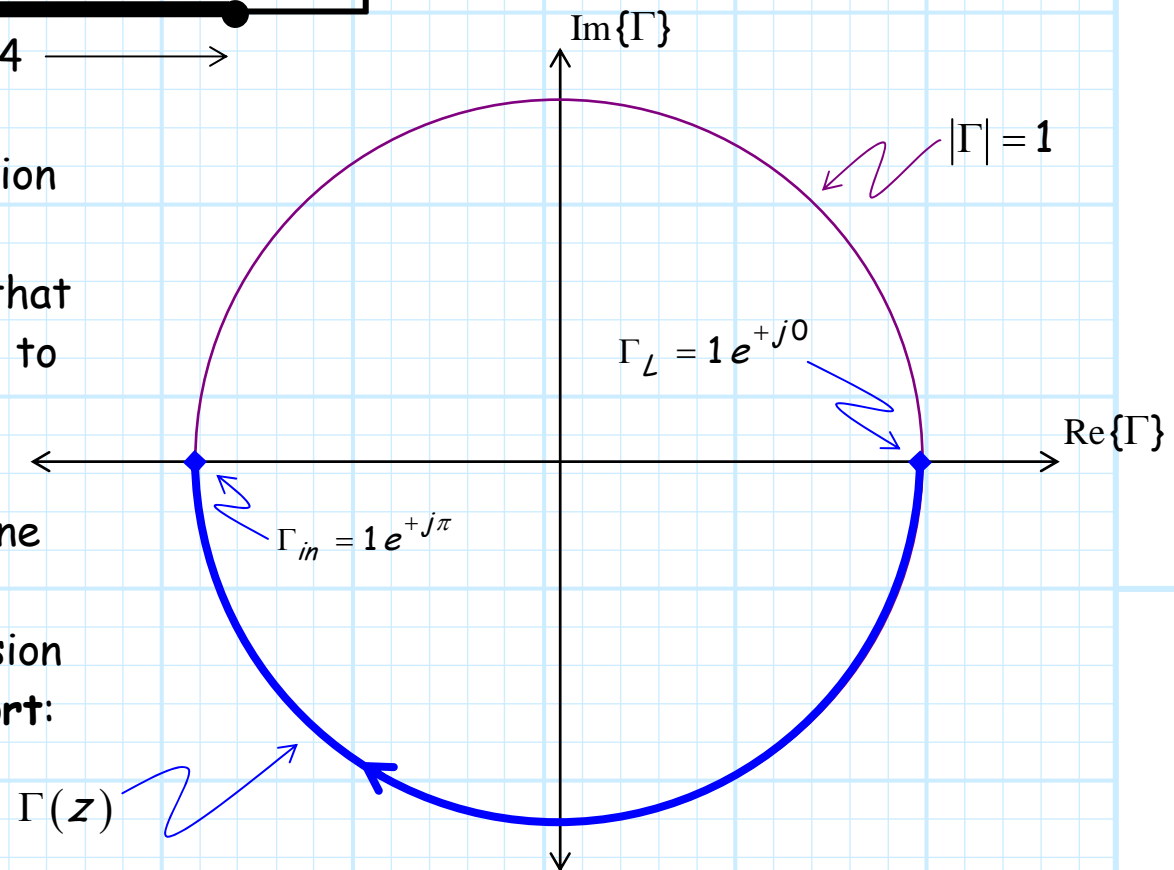
Our **short-circuit** load has been transformed into an **open** circuit with a **quarter-wavelength** transmission line!

## You're not surprised—are you?



Recall that a **quarter-wave** transmission line was one of the **special cases** we considered earlier. Recall we found that the input impedance was proportional to the **inverse** of the load impedance.

Thus, a **quarter-wave** transmission line transforms a **short** into an **open**. Conversely, a quarter-wave transmission can also transform an **open** into a **short**:



## Example: Now with $\ell = \lambda/2$

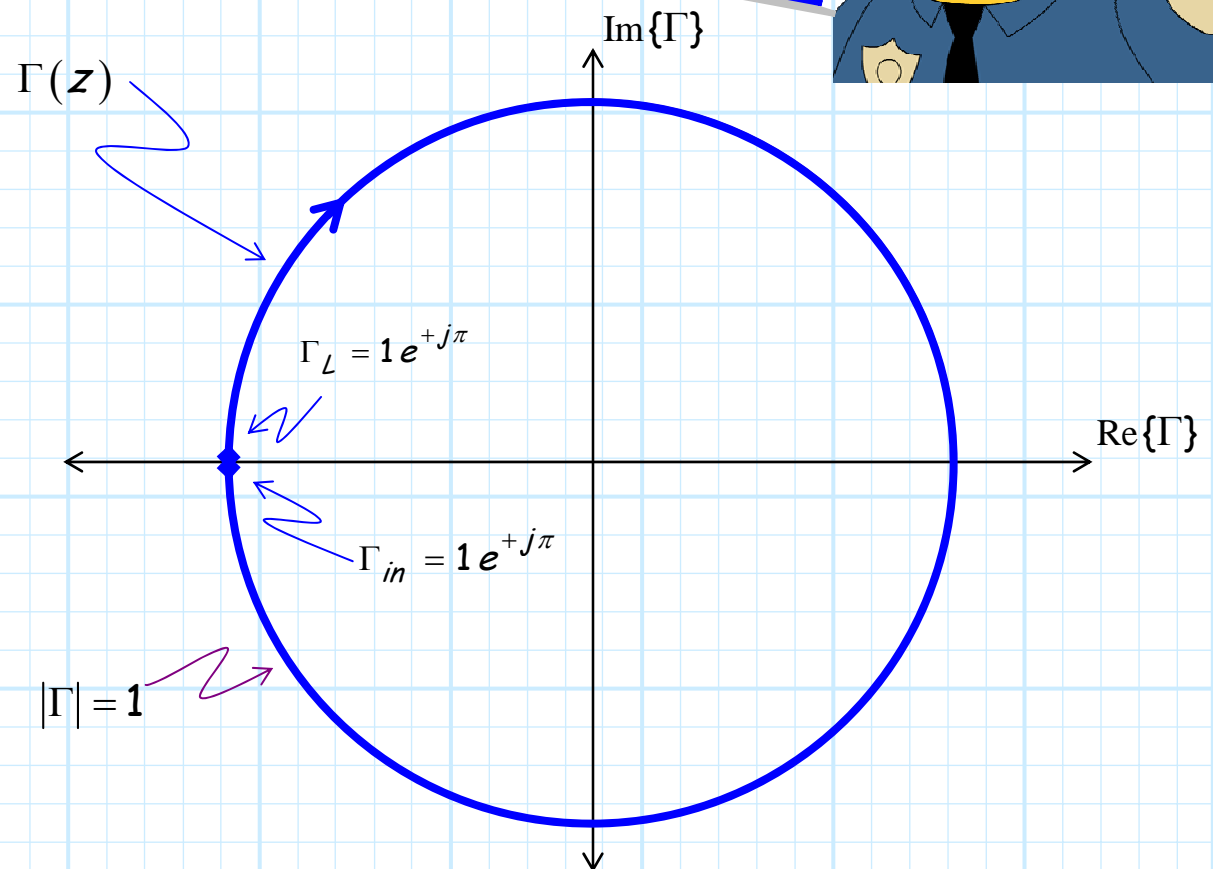
Finally, let's **again** consider the problem where  $\Gamma_L = -1$  (i.e., short), only this time with a transmission line length  $\ell = \lambda/2$  (a **half wavelength!**). We rotate **clockwise**  $2\beta\ell = 2\pi$  radians ( $360^\circ$ ).

*Hey look! We came clear around to where we started!*



Thus, we find that  $\Gamma_{in} = \Gamma_L$  if  $\ell = \lambda/2$ --but you knew **this** too!

Recall that the **half-wavelength** transmission line is likewise a **special case**, where we found that  $Z_{in} = Z_L$ . This result, of course, likewise means that  $\Gamma_{in} = \Gamma_L$ .



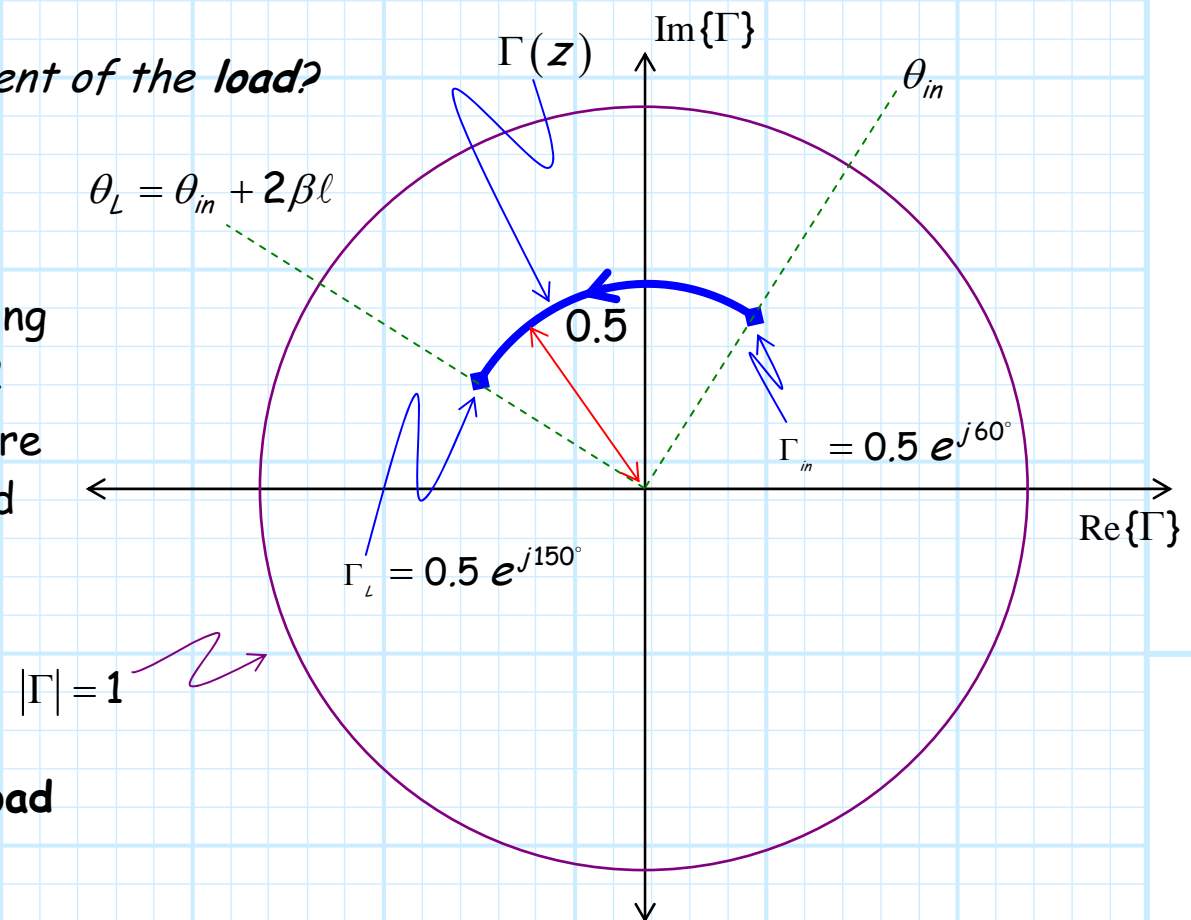
## Example: Now transform $\Gamma_{in}$ to $\Gamma_L$

Now, let's consider the **opposite** problem. Say we know that the **input** impedance at the **beginning** of a transmission line with length  $\ell = \lambda/8$  is:

$$\Gamma_{in} = 0.5 e^{j60^\circ}$$

**Q:** What is the reflection coefficient of the **load**?

**A:** In this case, we begin at  $\Gamma_{in}$  and rotate **COUNTER-CLOCKWISE** along a circular arc (radius 0.5)  $2\beta\ell = \pi/2$  radians (i.e.,  $60^\circ$ ). Essentially, we are **removing** the phase shift associated with the transmission line!



The reflection coefficient of the **load** is therefore:

$$\Gamma_L = 0.5 e^{j150^\circ}$$