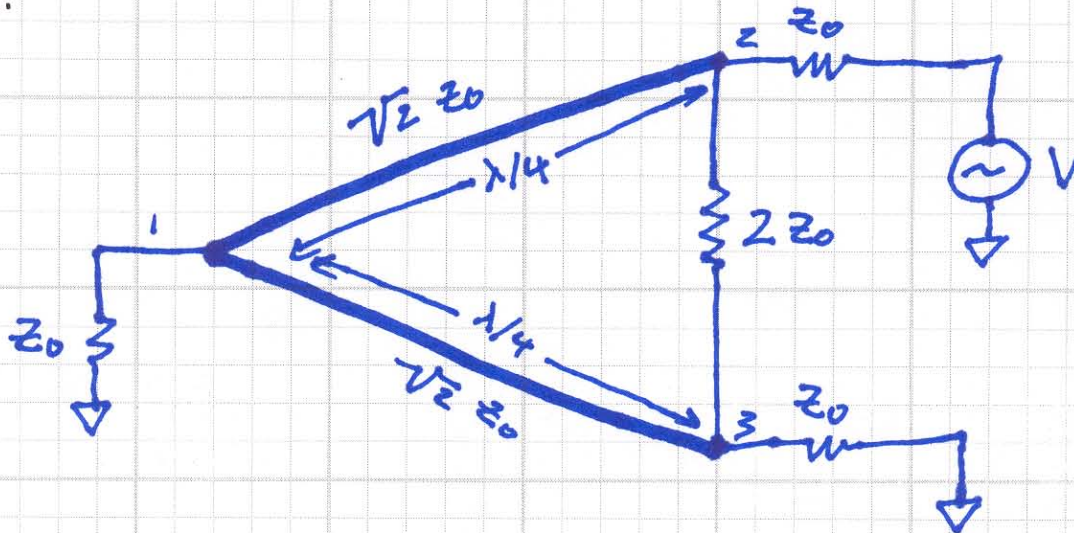


# Even and Odd Mode Analysis

Consider a matched Wilkinson power divider, with a source at port 2:



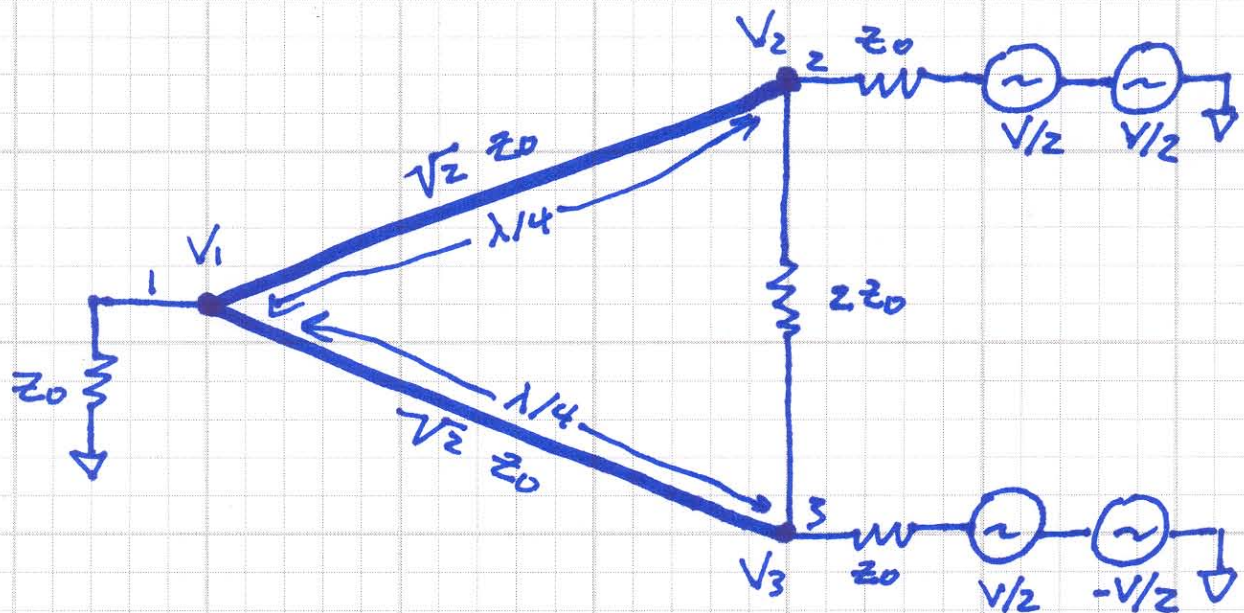
Q: How do we analyze this circuit?

A: Use Even-Odd mode analysis!

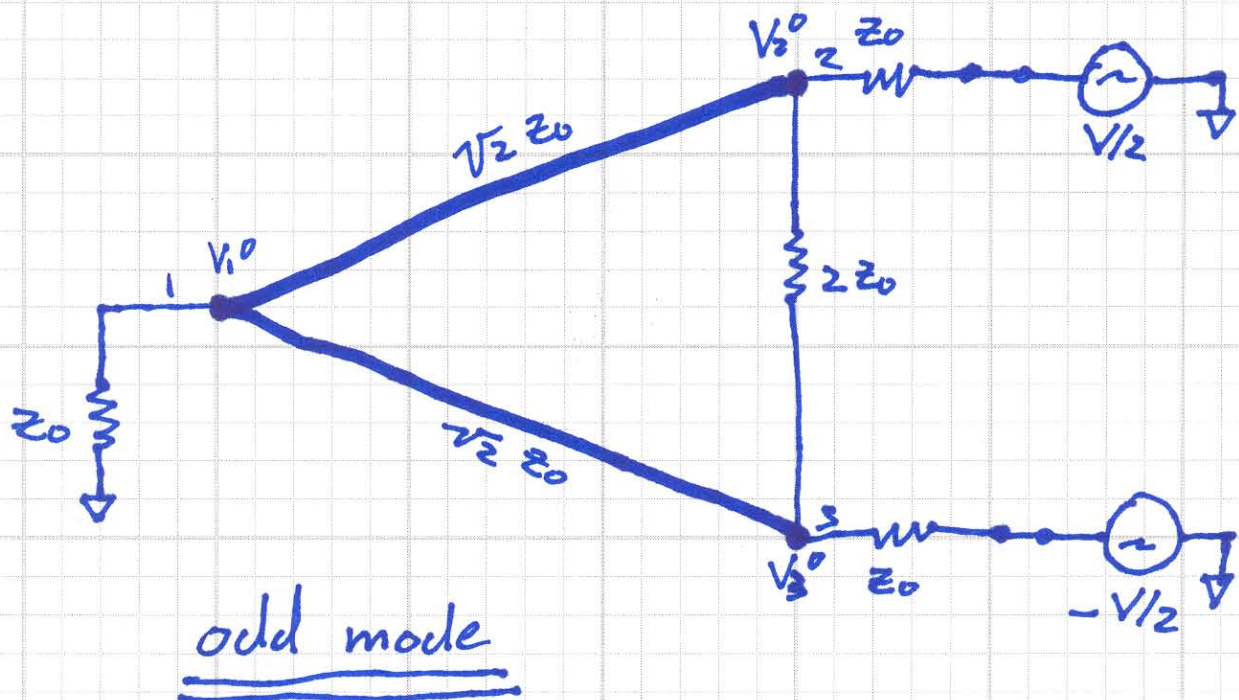
Even-Odd mode analysis uses two important principles:

- a) superposition
- b) circuit symmetry

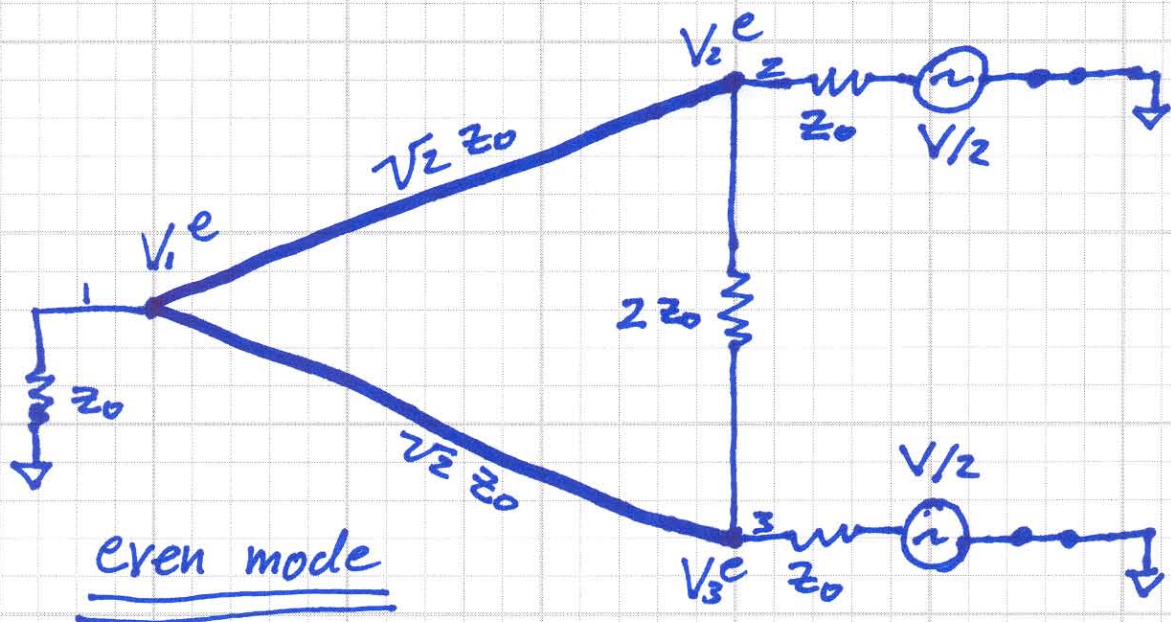
To see how we apply these principles, let's first rewrite the circuit with four voltage sources:



We can thus use superposition to determine all the currents and voltages within this circuit. We can first determine all **odd mode** currents and voltages:



And then determine all **even mode** voltages and currents:



And thus the voltages and currents within the circuit is simply the **sum** of the two modes:

$$V_1 = V_1^o + V_1^e$$

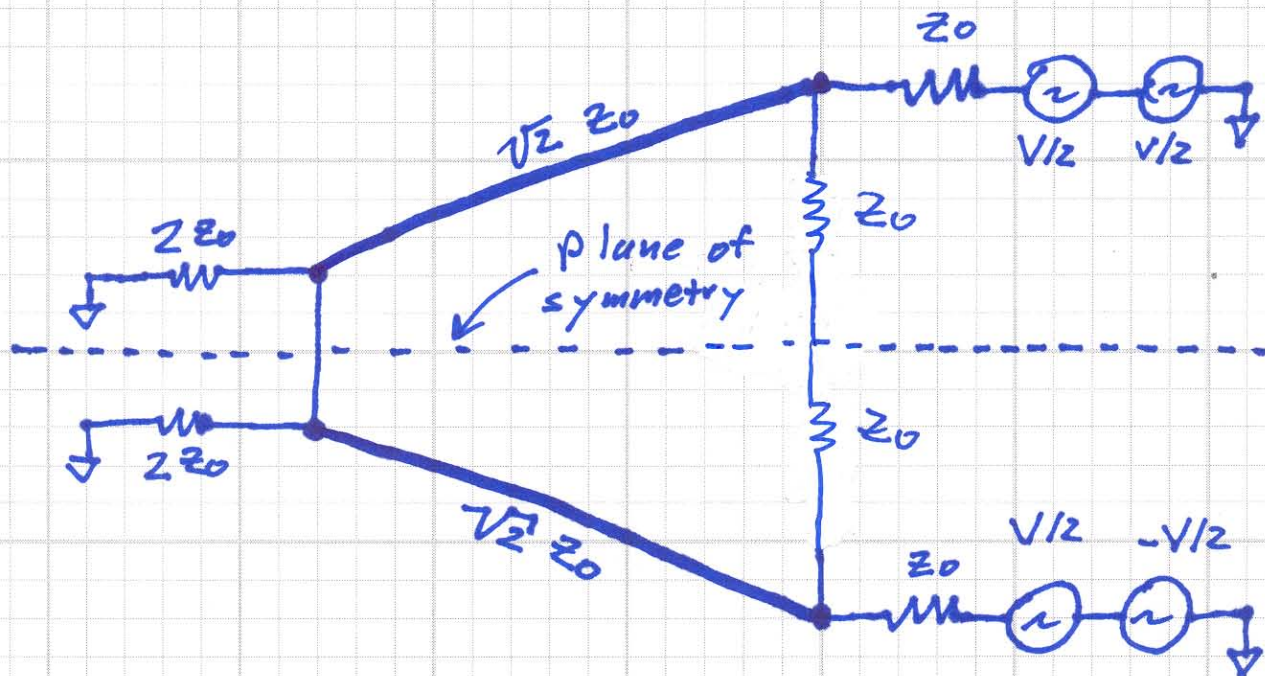
$$V_2 = V_2^o + V_2^e$$

$$V_3 = V_3^o + V_3^e$$

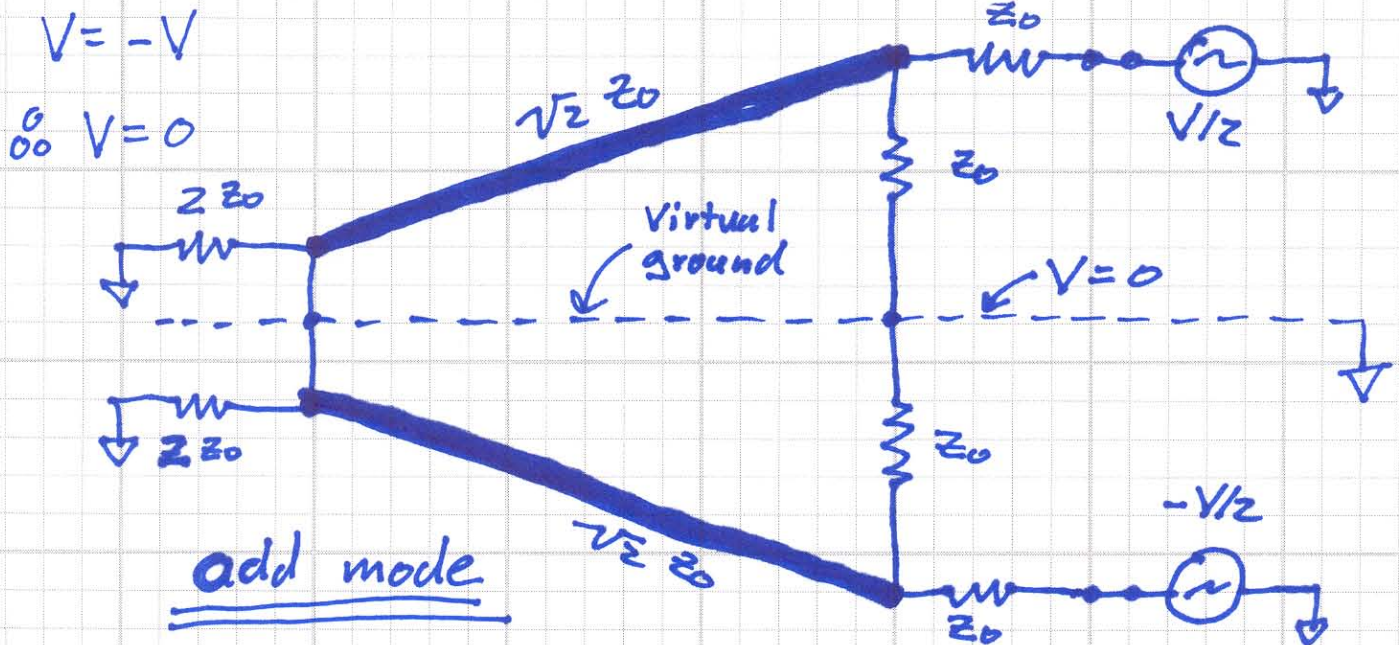
**Q:** *Yikes! Why in the world would we want to analyze a circuit this way? This "odd-even mode" analysis seems to just make things much harder!*

**A:** Be patient! We have yet to apply our second principle—**circuit symmetry**.

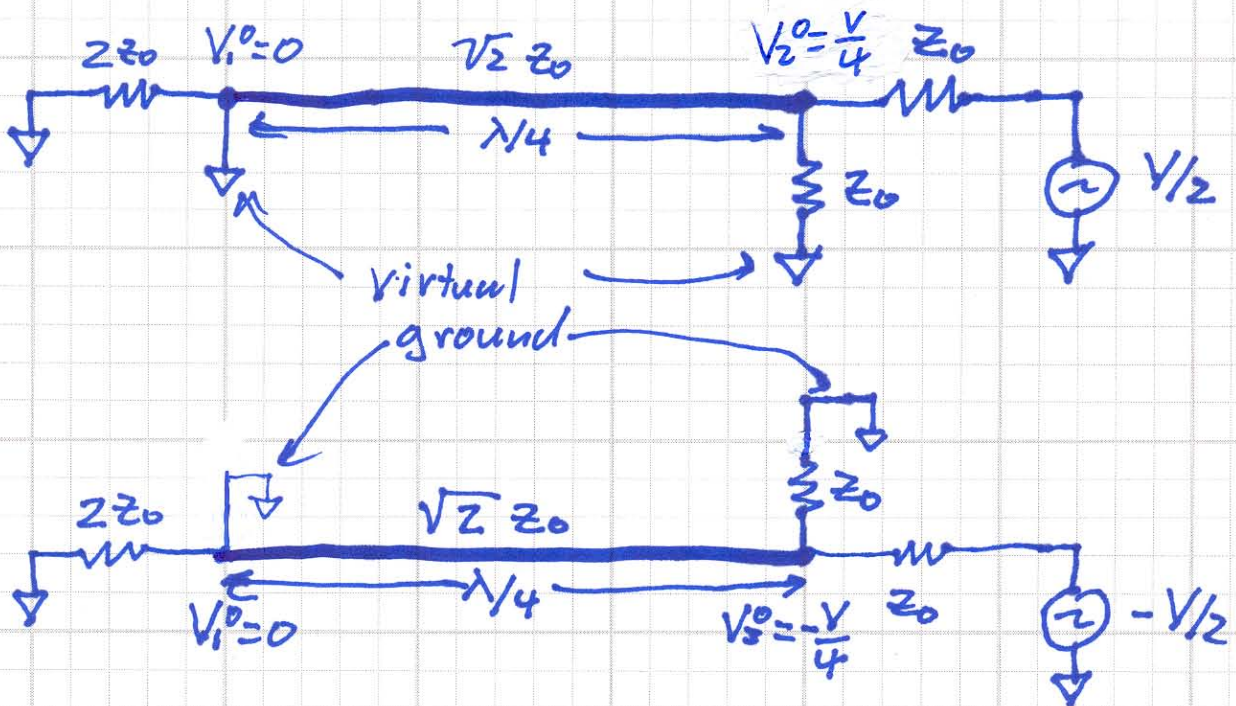
Note that we can rewrite the circuit with a perfect plane of circuit symmetry:



Consider now this symmetry with respect to the **odd mode**. It is evident that at **every** point along this symmetry plane, the **voltage must be zero!**

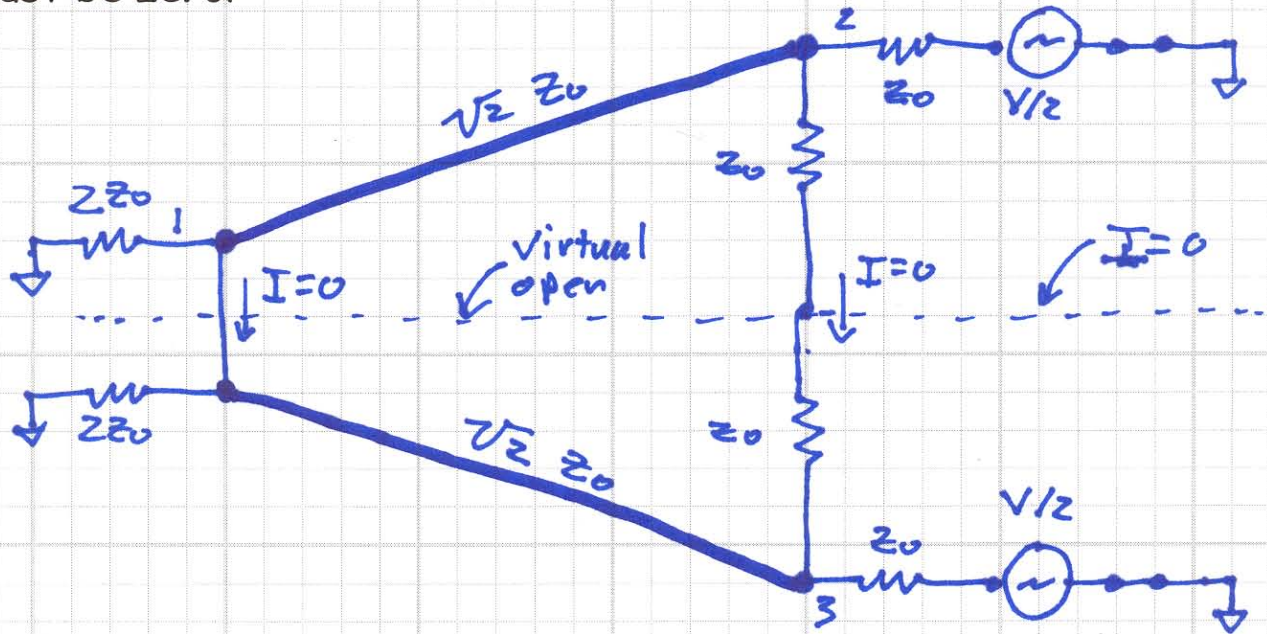


We call this odd mode symmetry plane a **virtual short**, as the voltage along this plane **must** be zero. As a result, we can divide the odd mode circuit into **two** pieces:

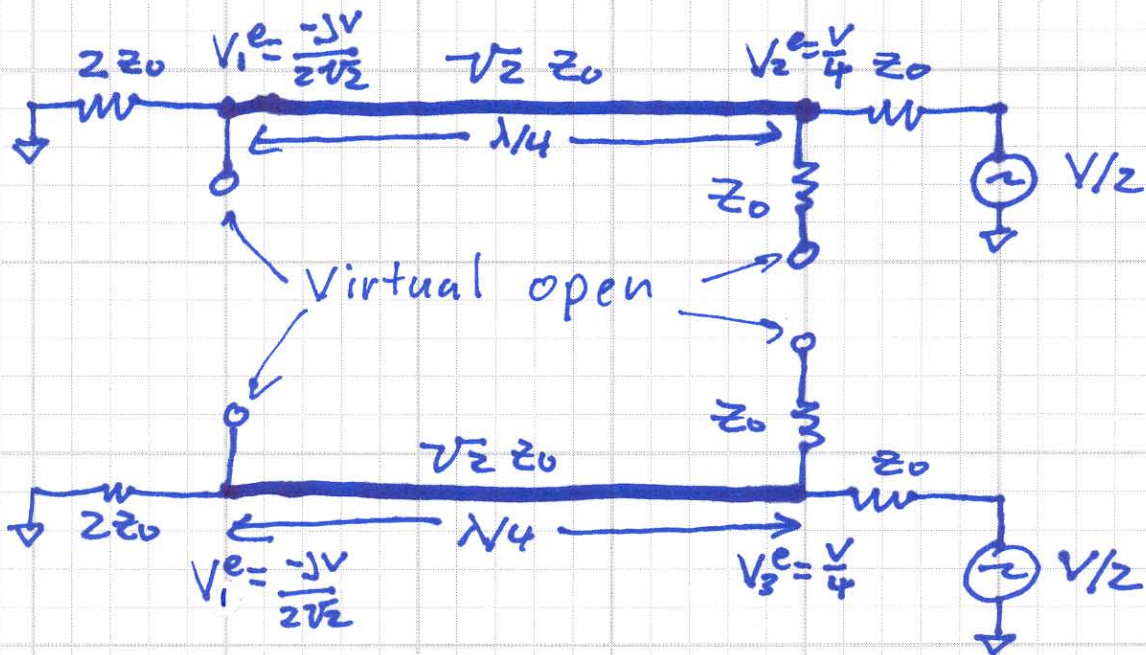


We can analyze these circuits!

Likewise, when we apply the **even mode** analysis, we find that at **every point** along this symmetry plane, the **current** crossing it must be zero!



We call this even mode symmetry plane a **virtual open**, as the **current** along this plane **must** be zero. As a result, we can divide the **even mode** circuit into **two** pieces:



Again, we know how to analyze each of **these** circuits!

Applying **superposition**, we can find the **total voltages** and **currents** by simply **adding** the results of each mode:

$$\begin{aligned} V_1 &= V_1^o + V_1^e \\ &= 0 + \frac{-jV}{2\sqrt{2}} = \frac{-jV}{2\sqrt{2}} \end{aligned}$$

$$\begin{aligned} V_2 &= V_2^o + V_2^e \\ &= \frac{V}{4} + \frac{V}{4} = \frac{V}{2} \end{aligned}$$

$$\begin{aligned} V_3 &= V_3^o + V_3^e \\ &= -\frac{V}{4} + \frac{V}{4} = 0 \end{aligned}$$

And from these results we can determine the following **scattering parameters**:

$$S_{22} = 0$$

$$S_{12} = \frac{-j}{\sqrt{2}}$$

$$S_{32} = 0$$

where  $V_2^+(z_2=0) = \frac{V}{2}$  ,  $V_1^-(z_1=0) = \frac{-j}{2\sqrt{2}}$

$$V_3^-(z_3=0) = 0 , \quad V_2^-(z_2=0) = 0$$

And from circuit **symmetry** and **reciprocity**, we can conclude:

$$S_{33} = 0$$

$$S_{21} = \frac{-j}{\sqrt{2}}$$

$$S_{23} = 0$$

$$S_{13} = \frac{-j}{\sqrt{2}}$$

$$S_{31} = \frac{-j}{\sqrt{2}}$$