4.4 - The Transmission Matrix

Reading Assignment: pp. 183-189

Let's now consider the **transmission matrix**—a matrix that can **only** be used to characterize a **two**-port device.

Q: Only for 2-port devices?!? That doesn't seem particularly useful. Why bother learning about this?

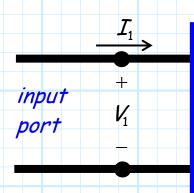
A: There are a lot of very important two-port devices (e.g., amplifiers, filters, attenuators).

HO: THE TRANSMISSION MATRIX

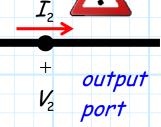
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The Transmission Matrix

If a network has **two** ports, then we can **alternatively** define the voltages and currents at each port as:



2-port Network



Q: Say, can we somehow relate the two input parameters (I_1, V_1) to the two output parameters (I_2, V_2) ?



A: Yes we can! We can relate them with four parameters A, B, C, D:

$$V_1 = A V_2 + B I_2$$

$$I_1 = C V_2 + D I_2$$

Or, using linear algebra:

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

The matrix is defined as the **transmission matrix** $\mathcal T$, otherwise known as the **ABCD matrix** :



 $\mathcal{T} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$

Q: Great. But what exactly **are** the values A, B, C, D, and how do we determine them?

A: Similar to the impedance and admittance matrices, we determine the elements of the transmission matrix using shorts and opens.



Note when $I_2 = 0$ then:

$$V_1 = A V_2$$

Therefore, to find value A, place an **open** on port 2, and then determine voltage V_1 in terms of V_2 . We find that:

$$A = \frac{V_1}{V_2} \quad \text{(port 2 open)} \quad \begin{array}{c} \frac{V_1}{V_1} \\ \frac{V_1}{V_2} \end{array}$$

Note the parameter A is unitless (i.e., it is a coefficient).

B

Note when $V_2 = 0$ then:

$$V_1 = B I_2$$

Therefore, to find value B, place a **short** on port 2, and then determine voltage V_1 in terms of I_2 . We find that:

$$B = \frac{V_1}{I_2} \quad \text{(port 2 short)} \quad \begin{array}{c} I_1 \\ + \\ V_1 \end{array}$$

Note parameter B has units of impedance (i.e., Ohms).

C

Note when $I_2 = 0$ then:

$$I_1 = C V_2$$

Therefore, to find value C, place an **open** on port 2, and then determine current I_1 in terms of voltage V_2 . We find that:

$$C = \frac{I_1}{V_2} \quad \text{(port 2 open)} \quad \begin{array}{c} I_1 \\ + \\ V_1 \end{array}$$

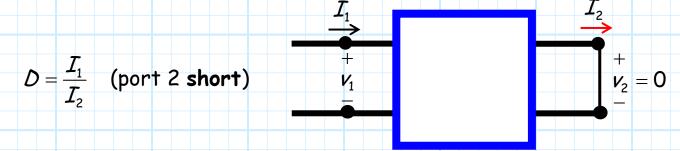
Note parameter Chas units of admittance (i.e., mhos).

D

Note when $V_2 = 0$ then:

$$I_1 = D I_2$$

Therefore, to find value D, place a **short** on port 2, and then determine current I_1 in terms of current I_2 . We find that:

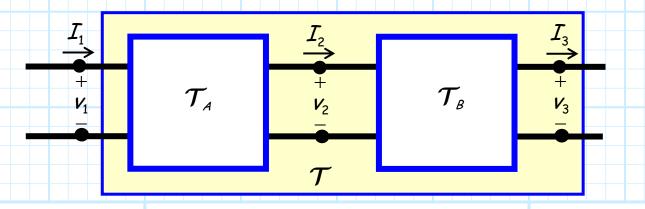


Note parameter D is unitless (another coefficient!).

Q: For cryin' out loud! We already have the impedance matrix, the scattering matrix, and the admittance matrix. Why do we need the transmission matrix also? Is it somehow uniquely useful?



A: Consider the case where a 2-port network is created by connecting (i.e., cascading) two networks:



Note

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \mathcal{T}_{\mathcal{A}} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

and

$$\begin{bmatrix} V_2 \\ I_2 \end{bmatrix} = \mathcal{T}_B \begin{bmatrix} V_3 \\ I_3 \end{bmatrix}$$

also

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \mathcal{T} \begin{bmatrix} V_3 \\ I_3 \end{bmatrix}$$

Combining the first two equations:

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \mathcal{T}_{\mathcal{A}} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix} = \mathcal{T}_{\mathcal{A}} \mathcal{T}_{\mathcal{B}} \begin{bmatrix} V_3 \\ I_3 \end{bmatrix}$$

and comparing to the third:

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \mathcal{T}_{A} \mathcal{T}_{B} \begin{bmatrix} V_3 \\ I_3 \end{bmatrix}$$
$$= \mathcal{T} \begin{bmatrix} V_3 \\ I_3 \end{bmatrix}$$

we conclude that:

$$\mathcal{T} = \mathcal{T}_{A}\mathcal{T}_{B}$$

Likewise, for N cascaded networks, the **total** transmission matrix $\mathcal T$ can be determined as the product of all N networks!

$$\mathcal{T} = \mathcal{T}_1 \, \mathcal{T}_2 \, \mathcal{T}_3 \, \mathcal{T}_4 \cdots \, \mathcal{T}_4 = \prod_{n=1}^N \mathcal{T}_n$$

Note this result is **only** true for the **transmission** matrix \mathcal{T} . No equivalent result exists for $\mathcal{S}, \mathcal{Z}, \mathcal{Y}$!

Thus, the transmission matrix can greatly **simplify** the analysis of **complex** networks constructed from **two**-port devices. We find that the \mathcal{T} matrix is particularly useful when creating design software for **CAD** applications.

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