

# Chapter 3 - Transmission Lines and Waveguides

First, some definitions:

**Transmission Line** - A **two** conductor structure that can support a **TEM** wave.

**Waveguide** - A **one** conductor structure that **cannot** support a **TEM** wave.

**Q:** *What is a **TEM** wave?*

**A:** An electromagnetic wave wherein **both** the electric and magnetic fields are **perpendicular** to the direction of wave propagation.

**HO: WAVEGUIDE**

## 3.5 Coaxial Line

**Reading Assignment:** p. 130

The most **prevalent** type of transmission line is the **coaxial** transmission line.

**HO: COAXIAL TRANSMISSION LINES**

Coaxial transmission lines are attached to devices using microwave connectors.

### HO: COAXIAL CONNECTORS

## 3.7 Stripline

**Reading Assignment:** pp. 137-140

Often, microwave devices or networks are built on dielectric substrates (e.g., "printed circuit boards"). Connecting these devices require printed circuit board transmission lines.

### HO: PRINTED CIRCUIT BOARD TRANSMISSION LINES

One of the most popular PCB transmission lines is stripline.

### HO: STRIPLINE

## 3.8 Microstrip

**Reading Assignment:** pp. 143-146

Another popular PCB transmission line is microstrip.

### HO: MICROSTRIP

## 3.11 Summary of Transmission Lines and Waveguides

**Reading Assignment: pp. 154-157**

Let's compare transmission line characteristics!

**HO: A COMPARISON OF COMMON TRANSMISSION LINES AND WAVEGUIDES**

# Waveguide

A waveguide is not considered to strictly be a transmission line, as it is **not** constructed with **two** separate conductors. As such, it can **not** support a TEM wave!

Instead, a waveguide will propagate "higher-order" **modes**, which are classified as either transverse magnetic (**TM**) or transverse electric (**TE**).

There are **two** problems with propagating higher-order modes!

- 1.** TE and TM modes have a **limited bandwidth**. In fact, none of these modes can propagate at frequencies below a minimum frequency known as the **cutoff frequency**.
- 2.** TE and TM modes are **dispersive**. That is, the phase velocity is dependent on frequency—for some modes highly dependent!

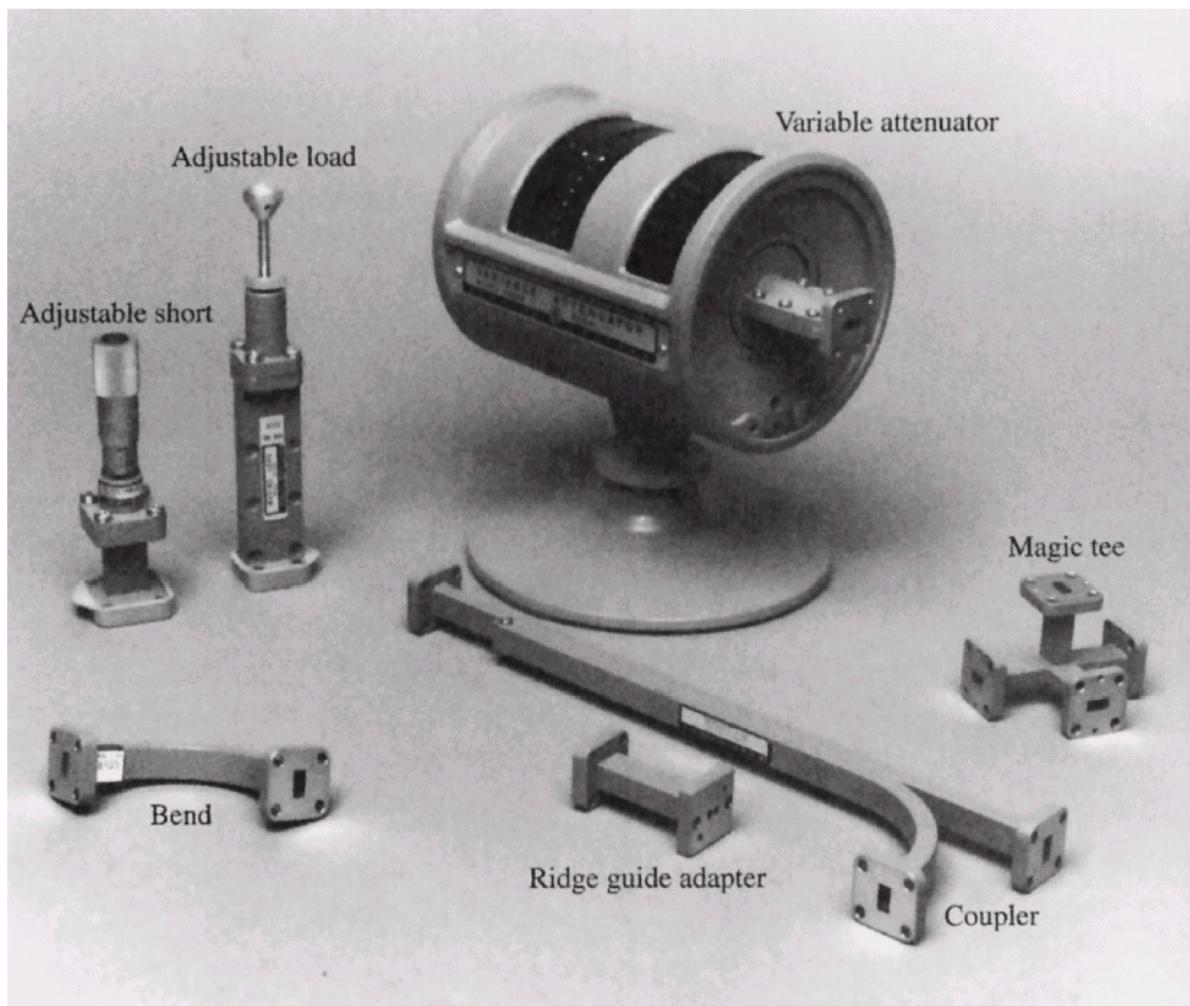
**Q:** Yikes! So why would we ever use a waveguide?

**A:** A waveguide likewise has **two** important **advantages**!

- 1.** It can typically handle **very large power** (e.g., kilowatts).
- 2.** It can have **very low loss** (low value of  $\alpha$ ).

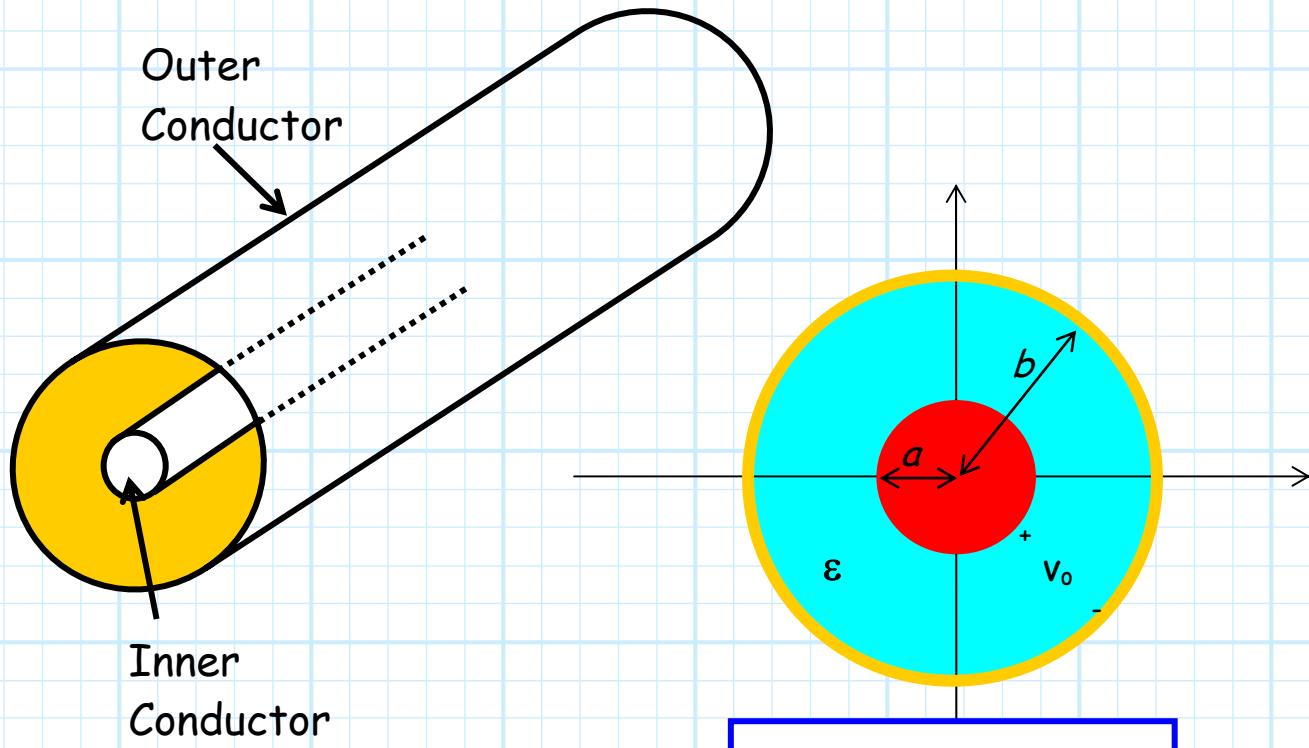
Thus, waveguide is typically used for **high-power** applications, such as high-power microwave transmitters.

Waveguide appears at first to simply be a **pipe** (either circular or rectangular), and effectively it is—an **electromagnetic pipe!**



# Coaxial Transmission Lines

The most **common** type of transmission line!

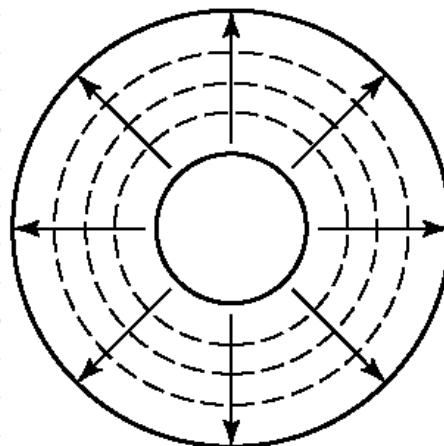


The **electric field** ( $\rightarrow$ ) points in the direction  $\hat{a}_\rho$ .

The **magnetic field** ( $- - -$ ) points in the direction  $\hat{a}_\phi$ .

E. M. Power flows in the direction  $\hat{a}_z$ .

→ A TEM wave!



Recall from EECS 220 that the **capacitance** per/unit length of a coaxial transmission line is:

$$C = \frac{2\pi\epsilon}{\ln[b/a]} \quad \left[ \frac{\text{farads}}{\text{meter}} \right]$$

And that the **inductance** per unit length is :

$$L = \frac{\mu_0}{2\pi} \ln \left[ \frac{b}{a} \right] \quad \left[ \frac{\text{Henries}}{\text{m}} \right]$$

Where of course the **characteristic impedance** is:

$$\begin{aligned} Z_o &= \sqrt{\frac{L}{C}} \\ &= \frac{1}{2\pi} \sqrt{\frac{\mu_0}{\epsilon}} \ln \left[ \frac{b}{a} \right] \end{aligned}$$

and:

$$\beta = \omega \sqrt{LC} = \omega \sqrt{\mu_0 \epsilon}$$

Therefore the **propagation velocity** of each TEM wave within a coaxial transmission line is:

$$v_p = \frac{\omega}{\beta} = \frac{1}{\sqrt{\mu_0 \epsilon}} = \frac{1}{\sqrt{\mu_0 \epsilon_0}} \frac{1}{\sqrt{\epsilon_r}} = c \frac{1}{\sqrt{\epsilon_r}}$$

where  $\epsilon_r = \epsilon/\epsilon_0$  is the relative dielectric constant, and  $c$  is the "speed of light" ( $c = 3 \times 10^8 \text{ m/s}$ ).

Note then that we can likewise express  $\beta$  in terms  $\epsilon_r$ :

$$\beta = \omega \sqrt{\mu_0 \epsilon} = \omega \sqrt{\mu_0 \epsilon_0} \sqrt{\epsilon_r} = \frac{\omega}{c} \sqrt{\epsilon_r}$$

Now, the **size** of the coaxial line ( $a$  and  $b$ ) determines **more** than simply  $Z_0$  and  $\beta$  ( $L$  and  $C$ ) of the transmission line. Additionally, the line radius determines the **weight** and bulk of the line, as well as its **power handling** capabilities.

Unfortunately, these two characteristics **conflict** with each other!

- 1.** Obviously, to **minimize** the weight and bulk of a coaxial transmission line, we should make  $a$  and  $b$  as **small** as possible.
- 2.** However, for a given line voltage, reducing  $a$  and  $b$  causes the **electric field** within the coaxial line to **increase** (recall the units of electric field are  $V/m$ ).

A higher electric field causes **two** problems: first, it results in greater **line attenuation** (larger  $\alpha$ ); second, it can result in **dielectric breakdown**.

Dielectric breakdown results when the electric field within the transmission line becomes so large that the dielectric material is **ionized**. Suddenly, the dielectric becomes a **conductor**, and the value  $G$  gets **very** large!

This generally results in the **destruction** of the coax line, and thus must be **avoided**. Thus, **large** coaxial lines are required when extremely **low-loss** is required (i.e., line length  $\ell$  is large), or the delivered **power** is large.

Otherwise, we try to keep our coax lines as **small** as possible!



# Coaxial Connectors

There are many types of **connectors** that are used to connect coaxial lines to RF/microwave devices. They include:



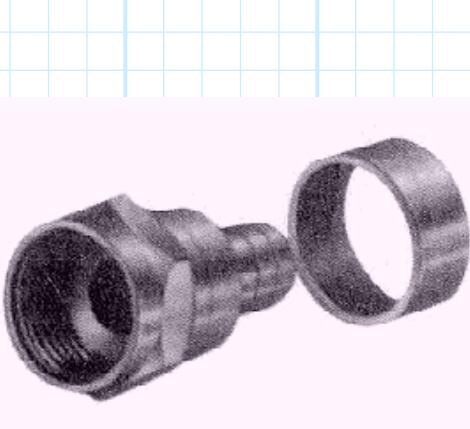
## SMA

The workhorse **microwave** connector. Small size, but works well to > 20 GHz. By microwave standards, moderately priced.



## BNC

The workhorse **RF** connector. Relatively small and cheap, and easy to connect. Don't use this connector past 2 GHz!



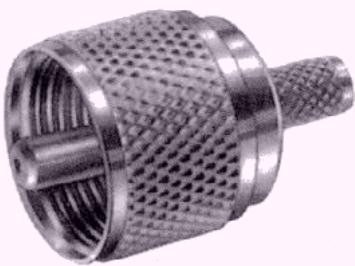
## F

A poorman's BNC. The RF connector used on most consumer products such as TVs. Cheap, but difficult to connect and not reliable.



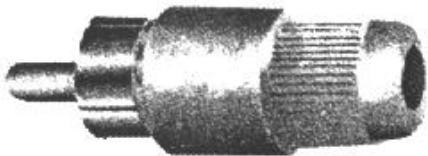
## N

The original microwave connector. Good performance (up to 18GHz), and moderate cost, but large (about 2 cm in diameter)! However, can handle greater power than SMA.



## UHF

The poorman's N. About the same size, although reduced reliability and performance.



## RCA

Not really an RF connector. Used primarily in consumer application for video and audio signals (i.e., <20 MHz). Cheap and easy to connect.



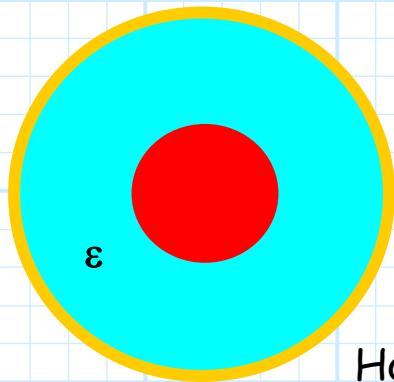
## APC-7 and APC-3.5

The top of the line connector. Best performance, but cost big \$\$. Used primarily in test equipment (e.g., network analyzers). 3.5 can work to nearly 40 GHz.

# Printed Circuit Board

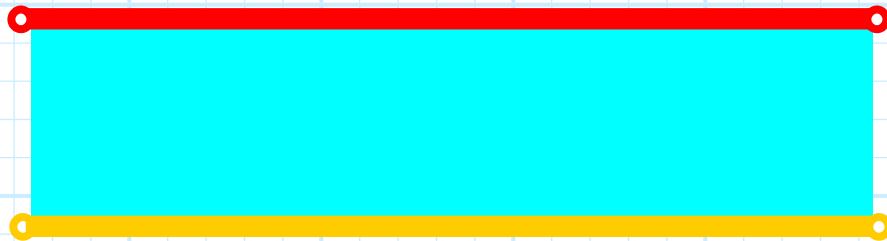
## Transmission Lines

Recall that a transmission line must consist of **two separate conductors**. Typically, the volume between these conductors is filled with a very low-loss **dielectric**.

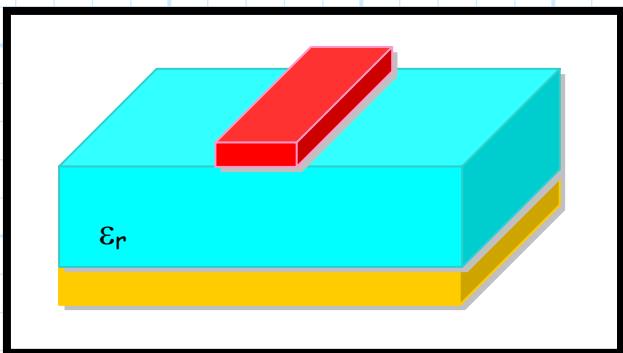


For example, a **coaxial** line has an inner conductor (**conductor #1**) and an outer conductor (**conductor #2**), with the cylindrical space between filled with dielectric.

However, we can likewise construct a transmission line using **printed circuit board** technology. The **substrate** of the circuit board is the dielectric that separates two conductors. The **first conductor** is typically a **narrow etch** that provides the **connection** between two components, while the **second conductor** is typically a **ground plane**.

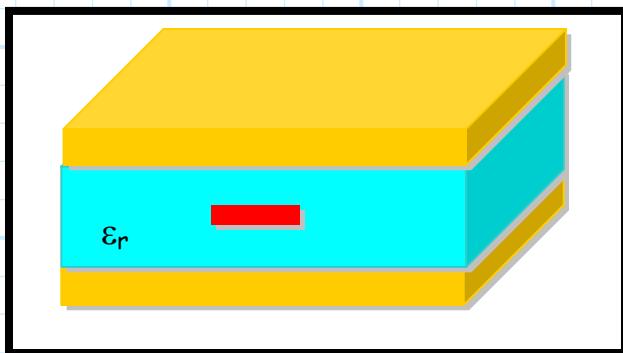


Below are some of the most popular types of printed circuit board transmission lines:



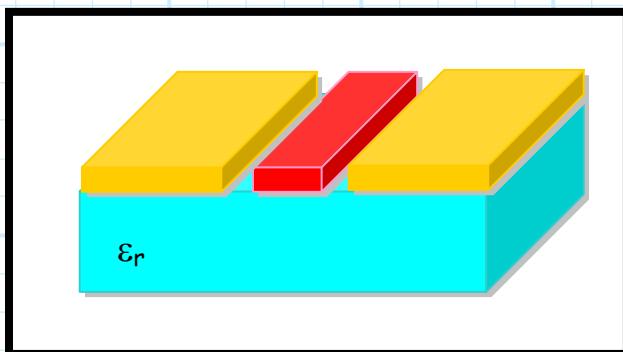
### Microstrip

Probably most popular PCB transmission line. Easy fabrication and connection, yet is slightly dispersive, lossy, and difficult to analyze.



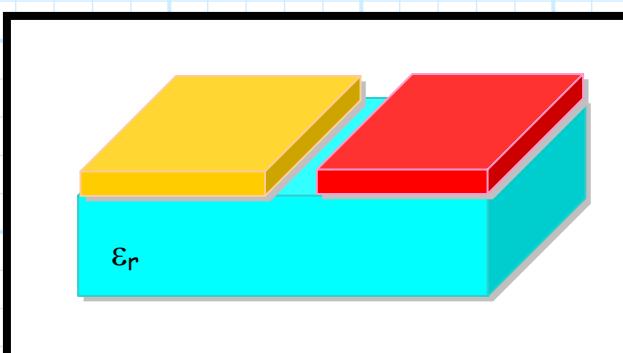
### Stripline

Better than microstrip in that it is not dispersive, and is more easily analyzed. However, fabrication and connection is more difficult.



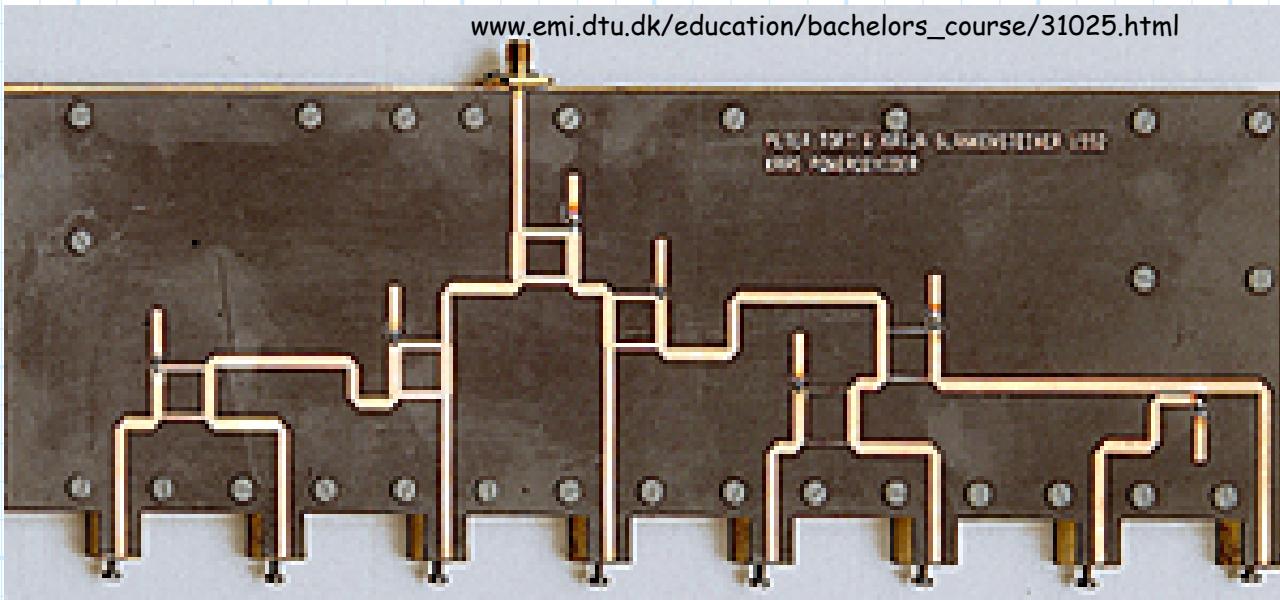
### Coplanar Waveguide

The newest technology. Perhaps easiest to fabricate and connect components, as both ground and conductor are on one side of the board.

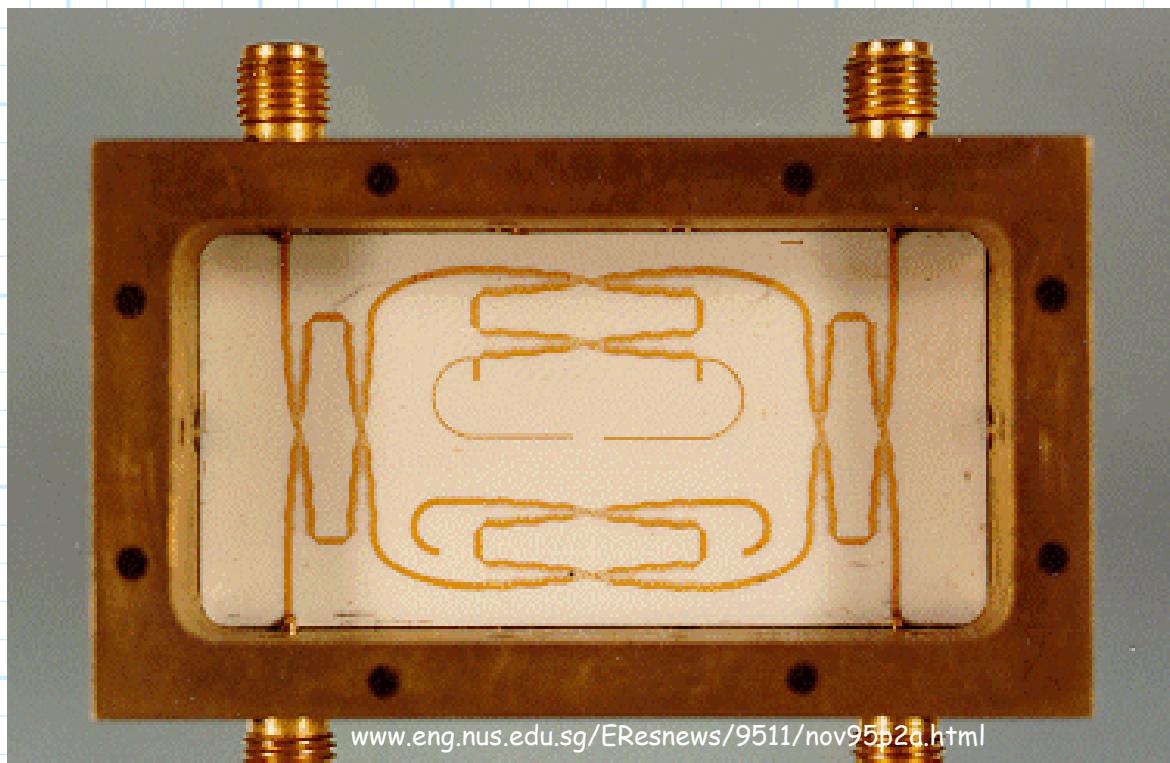


### Slotline

Essentially, a dual wire transmission line. Best for "balanced" applications. Not used much.



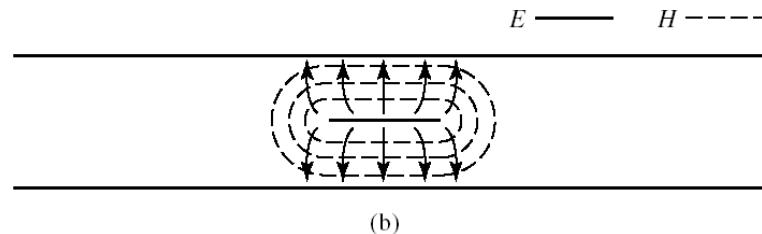
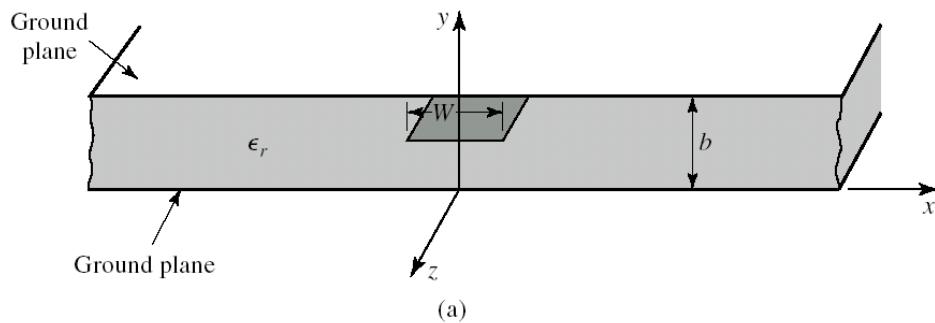
An antenna array feed, constructed using **microstrip** transmission lines and circuits.



A wideband **microstrip** coupler.

# Stripline Transmission Lines

Stripline—a TEM transmission line!



The characteristic impedance is therefore:

$$Z_o = \sqrt{\frac{L}{C}}$$

and:

$$\begin{aligned}\beta &= \omega\sqrt{LC} \\ &= \omega\sqrt{\epsilon\mu} \\ &= \frac{\omega}{c}\sqrt{\epsilon_r}\end{aligned}$$

However, there are no **exact** analytic solutions for the capacitance and inductance of stripline—they must be numerically analyzed. However, we can use those results to form an analytic **approximation** of characteristic impedance:

$$Z_0 = \frac{30\pi}{\sqrt{\epsilon_e}} \frac{b/W_e}{1 + 0.441 b/W_e}$$

where  $W_e$  is a value describing the **effective width** of the center conductor:

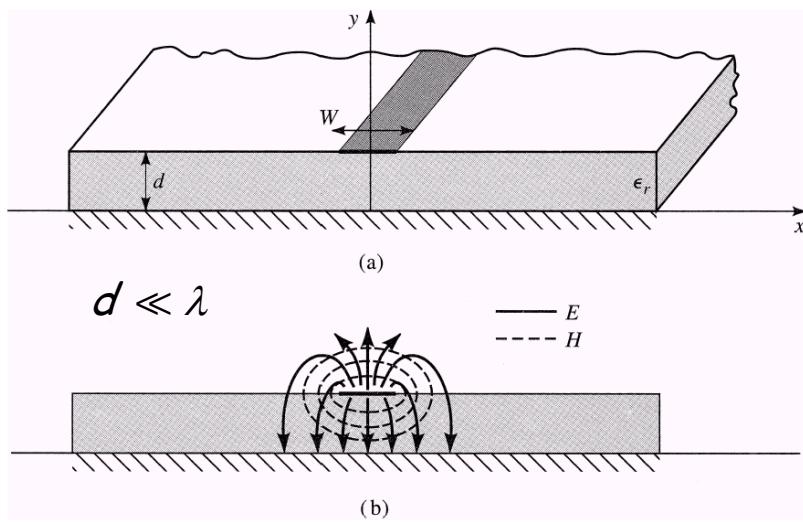
$$\frac{W_e}{b} = \frac{W}{b} - \begin{cases} 0 & \text{for } W/b > 0.35 \\ (0.35 - W/b)^2 & \text{for } W/b < 0.35 \end{cases}$$

Note that  $Z_0$  is expressed in terms of the **unitless** parameter  $W/b$ , a coefficient value **analogous** to the ratio  $a/b$  used to describe **coaxial** transmission line geometry.

From the standpoint of stripline **design**, we typically want to determine the value  $W/b$  for a desired value  $Z_0$  (i.e., the **inverse** of the equation above). This result is provided by equation 3.180 of your **textbook**.

# Microstrip Transmission Lines

Microstrip—a quasi-TEM transmission line!



There are no **exact** analytic solutions for a microstrip transmission line—they must be **numerically** analyzed. However, we can use those results to form an analytic **approximation** of microstrip transmission line behavior.

The propagation constant  $\beta$  of a microstrip line is related to its **effective relative dielectric**  $\epsilon_e$ :

$$\beta = \frac{\omega}{c} \sqrt{\epsilon_e}$$

where:

$$\epsilon_e = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \frac{1}{\sqrt{1 + 12 d/W}}$$

Note that  $\epsilon_e \neq \epsilon_r$ ; in fact,  $1 < \epsilon_e < \epsilon_r$ .

Likewise, the characteristic impedance of a microstrip line is approximately:

$$Z_0 = \begin{cases} \frac{60}{\sqrt{\epsilon_e}} \ln \left( \frac{8d}{W} + \frac{W}{4d} \right) & \text{for } W/d \leq 1 \\ \frac{120\pi}{\sqrt{\epsilon_e} [W/d + 1.393 + 0.667 \ln(W/d + 1.444)]} & \text{for } W/d \geq 1 \end{cases}$$

Note that both transmission line parameters are expressed in terms of the **unitless** parameter  $W/d$ , a coefficient value **analogous** to the ratio  $a/b$  used to describe **coaxial** transmission line geometry.

From the standpoint of microstrip **design**, we typically want to determine the value  $W/d$  for a desired value  $Z_0$  (i.e., the **inverse** of the equation above). This result is provided by equation 3.197 of your **textbook**.

# A Comparison of Common Transmission Lines and Waveguides

**Q:** Why don't we simply pick the **best** transmission line, and use it for **all** applications?

**A:** Every transmission line design has its pros and cons—**none** is the best for all applications, and each is best for **some** applications.

Table 3.6 provides an accurate list of these pros and cons:

Characteristic	Coax	Waveguide	Stripline	Microstrip
Preferred Mode	TEM	TE <sub>10</sub>	TEM	Quasi-TEM
Other Modes	TM, TE	TM, TE	TM, TE	TM, TE
Dispersion	None	Medium	None	Low
Bandwidth	High	Low	High	High
Loss	Medium	Low	High	High
Power Capacity	Medium	High	Low	Low
Physical Size	Large	Real Large	Medium	Small
Fabrication Ease	Medium	Medium	Easy	Real Easy
Component Integration	Hard	Hard	Fair	Easy